Centre universitaire d'étude des problèmes de l'énergie

# TRNSYS compatible moist air hypocaust model 

## Final report

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## Part 1 : Description and validation

## Introduction

## Preliminary work

History of this project draws back to a pilot project, also funded by the Federal Office of Energy, dealing with short term heat storage in agricultural greenhouses [4-6]. High involved humidities often induced condensation and evaporation within the hypocaust (pipe system). Sensitivity analysis therefore required a model that would take into account not only sensible but also latent heat exchanges, and allow for airflows in one or the other direction (for respect of thermal stratification during storage and withdrawal periods). Such a model had formerly been developped by Razafinjohany and Boulard [1] in the frame of a similar experience in Avignon, but happened not to be flexible in geometry outlay and input/output definition, nor to include possibilty of water infiltration - which in some cases will bee seen to play important role.

A first new development of the model was carried out within the mentioned project and allowed to reproduce general trends of condensation and evaporation patterns. A second validation work was done on a preheating system for fresh air in a residential building [8]. Monitoring could in this case be reproduced with an extremly good precision, but in absence of latent exchanges.

## Objectives

Since this had not yet been the case, main purpose of this project was to render the module compatible with the TRNSYS environment commonly used for simulation of energy sytems, in particular the possibility to link back and forth surface conditions with other modules that include thermal capacities, like buildings, and therefore to stand timestep iteration (one of the main features the TRNSYS environment uses for system convergence). Besides, further validation of the model was also to be done on yet another winter preheating and summer cooling system in a commercial building [9].

## Report structure

Body of this report will present essential features of the model (of which detailed description, including mathematical, is to be found in the user's manual). Focus will then be set on validation work for the three analysed systems.

## Overview of the model

## General features

The modeled hypocaust consists of a series of parallel tubes within a rectangular block of soil, swept by a flow of humid air. Flexible geometry description allows for inhomogenous soils, diverse border conditions, as well as use of symetries or pattern repetitions (run-time economy). Direction of the airflow can be controled (stratification in case of heat storage). Energy and mass balance within the tubes account for sensible as well as latent heat exchanges between airflux and tubes, frictional losses, diffusion into surrounding soil, as well as water infiltration and flow along the tubes.

## Sensible and latent heat exchange

Heart of the model and worthwile mentioning here is the energy exchange between air and tube, while three dimensional diffusive heat transfer within soil is of classical, explicit type.

Sensible exchange depends on the air-tube temperature difference and the exchange coefficent, latter one depending in turn on flowrate. Cutting short on more sophisticated use of dimensionless analysis, we used for this coefficient a heuristical form of linear dependence on air velocity (see mathematical description in the user's manual), as developped for large plane exchange surfaces [2] and proved to be consistent in case of tubes [6].

Latent heat exchange is based on the Lewis approach [3], which considers preceeding sensible heat exchange to be an air mass exchange between the airflux and a superficial air layer on tube surface, at latters temperature and saturated in humidity. This exchange of moist air conveys a vapor transfer (condensation or evaporation, according to sign of transfer) which readily computes from difference in humidity ratios (see mathematical description in the user's manual).

## Input/output configuration

Written as a TRNSYS compatible FORTRAN subroutine the model allows for modular use. Passed arguments include variable inputs (airflow, inlet temperature and humidity, air pressure, surface temperatures or heat gains) and fixed parameters that relate to either coupling with other modules (surface resistances and coupling modes) or simulation timestep and precision. Additional internal parameters (geometry, soil properties, initialisation, etc.) are furthermore provided by a parameter file. Retrieved arguments consist of basic outputs (outlet temperature and humidity, total sensible and latent heat rates, reciprocal border temperatures or heat gains) as well as a variety of optional outputs (including temperatures, energy rates and waterflows for specified node clusters).

## Coupling to other modules

In the case of simple links, output of some other module is connected to input of this module (e.g. ambient temperature connected to surface temperature of hypocaust, or outlet fan temperature connected to inlet temperature of hypocaust), without evolution of other module having any influence on present one. In the case of reciprocal linking, a second link goes back from hypocaust to other module, so that evolution of each module affects evolution of the other one (eg. diffusing energy rate from building ground is connected to energy rate entering at hypocaust surface, and reciprocaly border temperature of hypocaust is connected back to outside surface temperature of building ground).

In latter case convergence method by timestep iteration integrated into TRNSYS will ensure correspondance of energy rates flowing out of one module and into the other one (at condition of forth and back coupling to be each one of different type : energy rate or temperature). In order to maintain possibilities as broad as possible, each one of the two linking modes are retained: 1) input to surface is energy rate, reciprocal output is temperature ; 2 ) input to surface is temperature, reciprocal output is energy rate.

Checking of latter linking method as well as of proper energy and mass balance calculation within the module was done on an academic example presented in the user's manual.

## Validation on « Geoser » short term heat storage system in agricultural greenhouse

## System description

In the «Geoser» experiment [4-6] excessive solar heat gains of two greenhouses ( 100 m 2 ground surface each) in the Rhône valley were stored for reduction of fuel-consumption during heating period (usualy nightly). In the first case storage occured in a watertank (via an air/water heat exchanger), in the second case in the underlying and sidely isolated soil (via a burried pipe system), while a third greenhouse with mere fuel heating system served as a comparison.

The buried pipe heat storage system stands 80 cm underneath the greenhouse and consists of 24 tubes (external diameter : 16 cm ; length : 11 m ; mean axial distance : 42 cm ; total exchange surface, without distribution and collector pipes : $120 \mathrm{~m}^{2}$ ) swept by a variable airflow ( $0-7000 \mathrm{~m}^{3} / \mathrm{h}$ ) runing in one or the other direction during charge and discharge.

Typical daily operation is shown on figure 1: during lower setpoint period at night air from greenhouse is blown through pipes, takes up heat from soil and thus lowers demand to auxilary heating system. When difference between air and soil becomes too small for dischage (at setpoint change) system becomes inactive. As greenhouse temperature rises with solar radiation, air is blown again through pipes, this time for heat storage, in reversed direction, and until air-soil temperature difference becomes too small again. Same cycle repeats from sunset on.

During nightly discharge air heated along the tube evaporates free water in tubes, while storage period starts up with condensation of very moist greenhouse air, followed by evaporation again as air humidity drops down. Water balance shows a deficit (more evaporation than condensation) of 15 lit for this one day and of 800 lit over the 18 months of monitoring. This can most probably be explained by the use of a fog system at 2 m height within the greenhouse, which sprays droplets of $\sim 80$ microns into air. One clearly observes effect of fog system on air humidity and temperature, especially at 1 m height, when droplets reach wet bulb temperature and start to pump evaporation energy in air rather than in water and air (cf. detailed studies on atomization and spray phenomena [7,8]). According to data on sedimentation velocity and lifetime ( $\sim 20 \mathrm{~m} / \mathrm{s}$, respectively $3-40 \mathrm{~s}$ depending on air humidity, ibid.) it is quite plausible that part of the droplets are swept by airflow into tubes.


Fig 1: Operation of "Geoser » short term heat storage system on May $9^{\text {h }} 1994$ : conditions in greenhouse (air temperature, setpoints and humidity) and in soil (temperature near pipe), energy furnished to soil (sensible and latent), auxilary heat demand and fog system.

## Validation

Border and input conditions for modelling of this system are top and bottom temperatures $(40 \mathrm{~cm}$ above and 70 cm beneath pipes) averaged over two monitoring points each, as well as measured inlet temperature and humidity. Initialisation is done on first six monts of monitoring and 12 following months are used for comparison of simulation and monitoring (1/4/94-30/3/95).

As shown on figures 2 to 5 , a first simulation under preceeding conditions and without water infiltration very well reproduces sensible heat exchanges, as well in hourly as in integrated timestep. General trends of evaporation and condensation are beeing reproduced to some extent during first weeks (important measured latent exchanges, possibly due to use of only one air direction) but sytematically fall short in quantity and completely disappear at later periods. During first weeks one observes in particular (figure 3, broken line) that simulated latent exchange stops when condensed water has been evaporated again, which confirms the hypothesis of water infiltration during monitoring.

In a second simulation the measured daily water deficit is beeing infiltrated in constant hourly rate on the whole pipe surface, in which case evaporation (but not so condensation) is very well reproduced over the whole 12 month period.


Fig 2: Sensible energy rate (furnished to soil) for «Geoser» experiment : monitored and simulated data in hourly timestep from May $6^{h}$ to $16^{h}$ of 1994 (corresponding to $\sigma^{\text {th }}$ week of comparison period).


Fig 3: Latent energy rate (furnished to soil) for «Geoser» experiment: monitored and simulated data in hourly timestep from May $6^{h}$ to $16^{h}$ of 1994 (corresponding to $6^{h}$ week of comparison period).


Fig 4: Sensible energy rate (furnished to soil) for «Geoser» experiment : monitored and simulated data in weekly timestep over one year (April $1^{s t}$ to March 31 $1^{\text {st }}$ 1995).


Fig 5 : Latent energy rate (furnished to soil) for «Geoser» experiment : monitored and simulated data in weekly timestep over one year (April 1 ${ }^{s t}$ to March 31st 1995).

## Validation on «Caroubier» fresh air preheating system in a residential home

## System description

The «Caroubier» residential home in Geneva [9] is equiped with a complex preheating ventilation system in which, depending on solar radiation, fresh air passes either a solar roof or a burried pipe system before going through an exhaust air heat exchanger.

The hypocaust consists of 49 pipes (diameter : 12.5 cm ; lenghth : 50 m ; axial distance : 30 cm ; total pipe exchange surface : $980 \mathrm{~m}^{2}$ ) divided into two similar branches that are running at 50 cm beneath an underground parking, approximatly 10 cm above underground water level. Monitoring of the system over a 20 day winter period yields a two step airflow ( 1100 or $1400 \mathrm{~m}^{3} / \mathrm{h}$, for one of the two branches). No latent exchanges is detected over this period.

## Validation

Simulation of the system was to be carried out on a one year period. Initialisation and input conditions therfore were taken from standard yearly meteorological data, combined with monitored values of Geneva area during 3 months preceding monitoring period. Border condition at top was air in the parking lot (supposed to fluctuate between $7^{\circ} \mathrm{C}$ at end of February and $23^{\circ} \mathrm{C}$ at end of August), while temperature 2.5 m beneath pipes was supposed to be constantly at $15^{\circ} \mathrm{C}$ because of moving underground water.


Fig 6 : Sensible energy rate (furnished to soil) for "Caroubier» preheating system (one of the two branches) : monitored and simulated data in hourly timestep (March $9^{\text {th }}$ to $24^{\text {th }}$ of 1996).

Correspondence of simulated and measured data over short monitoring period (figure 6) results to be excellent despite of little constraints coming from monitoring. This fact is probably not so much inherent to the absence of latent exchanges than to oversizing of the system (all possible energy is exchanged over the pipe distance) and the presence of a constant heat source immediately underneath the pipes.

## Validation on «Schwerzenbacherhof» fresh air preheating and cooling system in a commercial and industrial building

## System description

Further checking was done by validating the model against monitoring data from the hypocaust system of the «Schwerzenbacherhof» office and commercial building [10], of which a set of hourly data over a one year period was handed out by the Federal Office of Energy.

The burried pipe system consists of 43 pipes (external diameter : 25 cm ; length : 23 m ; mean axial distance: 116 cm ; total exchange surface, including distribution and collector pipes : $900 \mathrm{~m}^{2}$ ) running at 75 cm beneath the second basement of the building ( $\sim 6 \mathrm{~m}$ beneath ground surface). A varying airflux during office hours ( $6^{\prime} 000-12^{\prime} 000 \mathrm{~m}^{3} / \mathrm{h}$ in winter, $18^{\prime} 000 \mathrm{~m}^{3} / \mathrm{h}$ in summer) yields winter preheating as well as summer cooling of the building.

Although not expicitly mentioned in the handed out report, infiltration of underground water seems to be at work all along the year : comparaison of mesured enthalpy balance with sensible heat exchange yields evaporation within the tubes all over the year (cf. figure 8 and 9 ), without any water deposit by condensation ever. More detailed analysis of the hypocaust energy balance however shows some inconsitency with other from monitoring derived data, which are heat diffusion from building and
towards deep ground ${ }^{1}$, as well as capacitive heat gains and losses ${ }^{2}$. As a matter of fact one observes resulting balance default to have same magnitude and dynamic as latent exchanges. This very strong corelation most probably draws back on some systematic error of inlet/outlet humidity sensors and a priori invalidates any conclusion on water flow (infiltration and evaporation).

## Validation

Border and input conditions for simulation of this system were upper soil temperature ( 75 cm above pipe bed, as averaged over 3 distinct monitoring points), lower soil temperature ( 600 cm beneath pipe bed, as given by a unique monitoring point), as well as inlet airflow, temperature and humidity. Initalisation was done by adding input data of last six months prior to effective yearly data.


Fig7 : Sensible and latent energy rates furnished to soil in «Schwerzenbacherhof» hypocaust system : monitored and simulated data in hourly timestep (22 ${ }^{\text {nd }}$ week of 1992).

A first simulation uses an hourly water infiltration of exactly the same amount than seemingly evaporated during monitoring. General trend of resulting hourly, weekly and seasonal dynamic compares generally speaking quite well with data from monitoring (cf. figures 7, 8 and 9), in particular water flows, since almost all infiltrated water is beeing evaporated with expected dynamic (but with a slight summer «storage» of free water within tubes, corresponding to 4 mm water on entire exchange surface, partly transfered on winter evaporation). Energy balance default from monitoring is mainly compensated by 1) increase in diffusion from building 2) decrease in diffusion to deep soil 3) lower winter preheating, respectively higher summer cooling (sensible exchange). Note that an altenative run with physicaly more plausible constant water infiltration yielded very similar results, not presented here.

A second simulation was done without water infiltration any (figures 7, 8 and 9). Except for evaporation which disapears completely, all other energy flows result to compare better to monitoring data than when infiltration is at work. This, as well as evolution of soil temperatures (figure 10) coroborates the hypothesis of inconsistency in monitoring of humidity.

[^0]



Fig 8: Energy rates (furnished to soil) for "Schwerzenbacherhof» system : monitoring and simulation (with and without water infiltration) in weekly timestep over one year (1992).


Fig 9 : Seasonal energy balance (plain flows, white and gray) and water balance (grey flows, plain and hatched) for "Schwerzenbacherhof» system: monitoring and simulation (with and without infiltration). Note that energy flow direction has nothing to do with air flow direction (summer sensible cooling power does not corespond to an airflow from building).


Fig 10: «Schwerzenbacherhof" ground temperatures: monitoring and simulation (with and without water infiltration) in weekly timestep over one year (1992).

Whatever reality might have been, mere comparison between each of these two simulations gives good understanding of the role water infiltration can play in such a sytem. Hence one observes presence of water and subsequent necessary heat for evaporation to lower winter preheating and to rise summer cooling of air, but only to some extent (changes account respectively for 20 and $28 \%$ of seasonal latent heat). Main influence goes for increase in heat diffusion from building (which accounts for $66 \%$ of latent heat in winter, respectively $58 \%$ in summer). Taken together, changes in air sensible heat and ground diffusion have an important consequence on building energy balance though. In winter, presence of water globaly lowers hypocaust performance of $50 \%$ (15.6-7.0 $0=8.6$ instead of $17.4-0.7=16.7 \mathrm{GWh}$ ). In summer on the contrary, presence of water globaly rises hypocaust performance of $50 \%(25.2+16.2=41.4$ instead of $16.4+11.8=28.2 \mathrm{GWh})$. This conclusion has nevertheless to be balanced by the fact that sensible heat carried by airflow can be distributed in a controled way, to the opposite of heat diffusion through ground.

## Conclusions

Validation on monitored systems shows that the developped hypocaust model, quite well reproduces latent and sensible heat exchanges of buried pipe systems, under condition of taking into account eventual presence of water infiltration. From a monitoring point of view, problematic seems rather to be the evaluation of such flows, while from a project designer point of view it rather is how to control them (tightness of systems). In this frame of idea the model might further on help to evaluate the consequences (risks and benefits) of water infiltration, whose effect relate in analysed cases not so much with outlet temperatures than with surface diffusion from coupled building.

Strictly speaking, some of the validation could gain to be reevaluated in presence of a reciprocal linking with the building, as developped and tested within this work on an academic example. Such a validation exercise would suppose a precise knowledge of the buildings enveloppe, heating/cooling and internal gain structure though.

Another interesting feature (used in sensitivity analysis of the «Geoser» experiment but not presented here) is the flexible geometry, in particular the possibility to simulate soil adjacent to the hypocaust (lateral losses) as well as the optional output structure. In this sense it could be interesting to perform a quite easy extension of the model to water instead of moist air medium, as is more and more commonly used.

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## References

1. Razafinjohany E., Etude comparative dans les serres agricoles de deux systèmes de stockage de la chaleur influencé de l'humidité de l'air, Thèse, 1989, Académie de Montpelier, Université de Perpignan.
2. Molineaux B., Lachal B., and Guisan O., Thermal analysis of five outdoor swimming pools heated by unglazed solar collectors, Solar Energy, Vol. 53, Nb. 1, July 1994, pp. 21-26.
3. Incropera F. P., De Witt D. P., Fundamentals of heat and mass transfer, John Wiley \& Sons Inc., 1990.
4. Lachal B., Hollmuller P., Gil J., Stockage de chaleur : résultats de GEOSER, in Stockage de chaleur, gestion de l'énergie et du climat dans les serres horticoles, recueil des exposés du colloque GEOSER du 15 février 1996 au RAC Conthey, Office fédéral de 1'énergie, 1996.
5. Lachal B., Hollmuller P., Gil J., Ergebnisse des GEOSER-Projekts, in Energie-Management im Gartenbau, Tagungsband zur Energiemanagement-Veranstaltung des 26. September 1996 an der ISW Wädenswil, Bundesamt für Energiewirtschaft, 1996.
6. Reist A., Lachal B., Jaboyedoff P., Hollmuller P., Gil J, GEOSER : stockage temporaire de chaleur pour serres horticoles, Rapport final (to be published).
7. Lefebvre A.H., Atomization and sprays, Hemisphere Publishing Corp., 1989.
8. Rodriguez E.A., Alvarez S., Martin R., Water drop as a natural cooling ressource : physical principles, PLEA Conference 1991, Kluver Academic Press, 1991, pp. 499-504.
9. Putallaz J., Lachal B., Hollmuller P., Pampaloni E, Evaluation des performances du puits canadien de l'immeuble locatif du 19 rue des Caroubiers, 1227 Carouge, expertise mandatée par l'Office cantonal de l'énergie de Genève, 1996.
10.Zimmermann M., The Schwerzenbacherhof Office and Industrial Building, Switzerland. Ground Coupled Ventilation System, IEA Low Energy Cooling Task, 1995.

# TRNSYS compatible moist air hypocaust model 

## Part 2 : User manual

## TYPE 61 : HYPOCAUST (AIR-TO-SOIL EXCHANGER)

## General Description

This component models an air-to-soil heat exchanger. It accounts for sensible as well as latent exchanges between airflux and tubes, diffusion into surrounding soil, frictional losses and flow of condensed water along the tubes. Local heating from integrated fan motor can be taken into account at tube inlet or outlet. Direction of airflux can be controled (stratification in case of heat storage) and flexible geometry allows for inhomogenous soils as well as diverse border conditions.

## Nomenclature

List hereafter covers all symbols used in the mathematical description of the model (other symbols are defined directly in the component configuration section). When as here, symbols in text account for currently described node and timestep, while subsripts are used to reference neighbor nodes or previous timestep.

| ClatWat | Latent heat of water |
| :--- | :--- |
| CmAir | Mass-specific heat of air |
| CmVap | Mass-specific heat of vapor |
| CmWat | Volume-specific heat of water |
| CVSoil | Volume-specific heat of soil |
| CVTub | Volume-specific heat of tube |
| Ctub | Circumference of tube |
| Dt | Internal timestep |
| Dl | Node width (along x, y or z) |
| Dtub | Hydraulic diameter of tube |
| Fair | Airflow in tube |
| FairTot | Airflow, total (over tubes and modules) |
| Hrel | Relative humidity |
| Hrat | Absolute humidity (vapor pressure) |
| Hsat | Absolute humidity (vapor pressure) at saturation |
| Kair | Air/tube exchange coefficient |
| Kbord | Heat conduction coefficient of border (pondered, including Rsurf) |
| Ksoil | Heat conduction coefficient to neighbour node or surface (including Rsurf) |
| LamSoil | Heat conductivity of soil |
| LamTub | Heat conductivity of tube |
| MmolAir | Molar mass of air |
| MmolWat | Molar mass of water |
| Mair | Mass of air exchanged between airflow and tube superficial layer |
| Mwat | Mass of free water |
| MwatIn | Mass of water flowing into node |
| MwatInf | Mass of water infiltrating into node |
| MwatLat | Mass of water cond./evap. |


| MwatOut | Mass of water flowing or ejected out of node |
| :--- | :--- |
| Pfric | Energy rate of frictional losses |
| Pint | Energy rate of tube or soil internal gains |
| Plat | Energy rate of latent air-tube heat exchange |
| Psbl | Energy rate of sensible air-tube heat exchange |
| Psoil | Energy rate of heat diffused by neighbor nodes |
| Pwat | Energy rate of free water internal losses |
| PrAir | Pressure of air |
| Rsurf | Surface heat resistance |
| Rfric | Friction coefficient of tubes |
| RhoAir | Specific weight of air |
| Sair | Section of tube |
| Sbord | Area of border |
| Ssoil | Lateral area of soil node |
| Stub | Lateral area of tube node |
| Tair | Temperature of air |
| Tbord | Pondered temperature of border |
| Tsoil | Temperature of soil |
| Ttub | Temperature of tube |
| ThTub | Thickness of tube |
| Vair | Air velocity |
| Vwat | Velocity of water |
| VolSoil | Node volume |
| VolTub | Volume of tube node |
| Hrat | Humidity ratio |

## Mathematical Description

## Geometry

The model describes a block of rectangular soil nodes (which need not all share same physical properties), comprising parallel tubes that run along the x -axis (see figure 1). A correction factor allows to describe non-rectanguar tubes. If not adiabatic, surface conditions (which need not expand from edge to edge) can be given in terms of either inflowing energy rate or temperature. An additional surface resistance can be defined, especially for direct coupling with air temperature.
For matter of simplification and run time economy, symetries in the $y-z$ plane can be used by describing only one module (=relevant part) and specifying the number of times it is used. In this case the symetry surface(s), which must be subject to adiabatic condition, may if necessary pass through the middle of some tubes (see figure 1).
Parametrisation of chosen geometry occurs in following way (of which best understanding can be taken from figure 1 and example at end) :

- define the occurence of typical cross-sections along the $x$-axis, with numbers that refer to them.
- define the typical cross-sections in the y-z plane, with numbers that refer to soil types, respectively surface conditions.
- define two additional cross-sections for frontal and rear surface conditions.


Hypocaust (Type 61)
b) cross-section \# 2 (through both zones)

parametrisation (by symetry only left half) :
$\left.\begin{array}{lllllllllllllll} & 3 & 3 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & \\ 0 & 1 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 0 \\ 0 & 1 & 2 & 2 & 0 & 2 & 2 & 2 & 0 & 2 & 2 & 2 & 0 & 0 \\ 0 & 1 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 0 \\ 0 & 1 & 2 & 2 & 2 & 2 & 0 & 2 & 2 & 2 & 0 & 2 & 2 & 0 \\ 0 & 1 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 0 \\ 0 & 1 & 2 & 2 & 0 & 2 & 2 & 2 & 0 & 2 & 2 & 2 & 0 & 0 \\ 0 & 1 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 2 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0\end{array}\right]$

Fig.1: Example of Type61 geometry and coupling to other Type.

## Linking

In addition to airflow at inlet/outlet, surface conditions can also be coupled to other Types. One can therefore choose between following two modes :

- If output from other module (=input for Type 61) is the energy rate flowing into hypocaust, Type61 will return equivalent border temperature as output (=input for other Type). Latter is defined as the pondered average node temperature of all nodes comprised in that particular surface :

$$
\begin{equation*}
\text { Tbord }=\frac{\sum_{i \in \text { bord }} \text { Ssoil }_{i} \cdot \text { Ksoil }_{i} \cdot \text { Tsoil }_{i}}{\text { Sbord } \cdot \text { Kbord }} \tag{1}
\end{equation*}
$$

with

$$
\text { Ksoil }_{i}=\frac{1}{\frac{D l_{i} / 2}{\text { LamSoil }_{i}}+\text { Rsurf }}
$$

$$
\begin{aligned}
& \text { Sbord }=\sum_{i \in b o r d} \text { Ssoil }_{i} \\
& \text { Kbord }=\frac{\sum_{i \in b o r d} S s o i l_{i} \cdot \text { Ksoil }_{i}}{S \text { Sord }}
\end{aligned}
$$

One has to take care to use identical border area Sbord and heat conduction coefficient Kbord in other Type (check these calculated values in parameter control file). The timestep iteration procedure of TRNSYS then will guarantee for proper energy balance (energy rate flowing out of one module $=$ energy rate flowing into other module), which can be checked by plotting inflowing energy rate as optional output of Type 61.

- If on the contrary output from other module is its equivalent border temperature, Type61 will return inflowing energy rate as output. Proper energy balance again is guaranteed by using identical border area and heat conduction coefficient in both Types.


## Air flow

Air flow is either positive, negative or zero. If modelling a set of tubes of distinct cross sections, total flow is distributed among the tubes in following way:

$$
\begin{equation*}
\text { Fair }=\text { FairTot } \cdot \frac{\text { Sair } \cdot \sqrt{D t u b}}{\sum_{\text {tubes }}(\text { Sair } \cdot \sqrt{D t u b})} \tag{2}
\end{equation*}
$$

so that according to form of pressure losses (see equation 12 further on) pressure equilibrium at output as well as power and flow integrals are respected.

## Water flow

Apart from condensation of airflow (see air-tube heat exchange, further on), water can also enter tubes by infiltration (along part or all of the tube surface). Resultant free water either flows along the tubes or is directly ejected out of hypocaust (flow/ejection occurs in same direction than airflow, in positive direction when airflow is zero). Water flowing/ejected out of a tube node is :

$$
\text { MwatOut }= \begin{cases}\left(M w a t_{t-1}+\Delta M w a t\right) \frac{V w a t \cdot D t}{D l} & \text { if water is flowing }  \tag{3}\\ \left(M w a t_{t-1}+\Delta M w a t\right) & \text { if water is ejected }\end{cases}
$$

where

$$
\Delta M w a t=\text { MwatIn }+ \text { MwatInf }+ \text { MwatLat }
$$

while water flowing from preceeding node ( $\mathrm{i} \pm 1$, depending on flow direction) into actual one is :

$$
\text { MwatIn }= \begin{cases}\text { MwatOut }_{i \pm 1} & \text { if water is flowing }  \tag{4}\\ 0 & \text { if water is ejected }\end{cases}
$$

## Air-tube heat exchange

In each tube node, from inlet towards outlet, following heat exchanges are taken into account :

- Sensible heat is caracterised by a an exchange coefficient which depends on flowrate. Cutting short on dimensionless analysis, the model uses a linear dependence on air velocity (as derived from experiences on large plane surfaces [3] and confirmed by the author in the frame of an experience on a burried pipe system).

$$
\begin{equation*}
\text { Kair }=\text { Kair0 }+ \text { Kair } 1 \cdot \text { Vair } \tag{5}
\end{equation*}
$$

so that

$$
\begin{equation*}
\text { Psbl }=\text { Stub } \cdot \text { Kair } \cdot(\text { Tair }- \text { Ttub }) \tag{6}
\end{equation*}
$$

- Latent heat is determined by the Lewis approach [4] which considers preceeding sensible heat exchange to result from an air mass exchange between the airflux and a superficial air layer on the tube surface, at latters temperature and saturated in humidity. Analogy between heat and mass transfer readily give exchanged air mass during timestep $D t$ :

$$
\text { Mair }=\frac{\text { Psbl } \cdot \text { Dt }}{\text { CmAir } \cdot(\text { Tair }- \text { Ttub })} \text {, }
$$

that is

$$
\begin{equation*}
\text { Mair }=\frac{\text { Stub } \cdot \text { Kair } \cdot \text { Dt }}{\text { CmAir }} \tag{7}
\end{equation*}
$$

This air exchange conveys a vapor transfer, which is determined by the difference of humidity ratios of the airflux and the saturated layer :

$$
\begin{align*}
\text { MwatLat } & =(\text { Hrat }(\text { Tair, Hrel })-\operatorname{Hrat}(\text { Ttub,100\% })) \cdot \text { Mair } \\
& =\left(\operatorname{Hrat}(\text { Tair, Hrel })-\operatorname{Hrat}(\text { Ttub,100\%) }) \cdot \frac{\text { Stub } \cdot \text { Kair } \cdot D t}{\text { CmAir }}\right. \tag{8}
\end{align*}
$$

where, from equation of perfect gazes, humidity ratio computes as

$$
\begin{equation*}
\text { Hrat }(T, \text { Hrel })=\frac{\text { Hsat }(\text { Tair }) \cdot \text { MmolWat }}{\text { PrAir } \cdot \text { MmolAir }} \tag{9}
\end{equation*}
$$

According to its sign, this vapor transfer corresponds to condensation (MwatLat $>0$ ) or evaporation (MwatLat < 0). In latter case MwatLat is furthermore limited by 1) available free water in node and 2) saturation pressure of air. Latent heat exchange is finally expressed as

$$
\begin{equation*}
\text { Plat }=\text { Clat } \cdot \frac{M w a t L a t}{D t} \tag{10}
\end{equation*}
$$

- Diffused heat from surrounding nodes (4 soil nodes, 2 tube nodes) is given by

$$
\begin{equation*}
\text { Psoil }=\sum_{i=1}^{6} \text { Ssoil }_{i} \cdot \text { Ksoil }_{i} \cdot\left(\text { Tsoil }_{i, t-1}-\text { Ttub }\right) \tag{11}
\end{equation*}
$$

where

$$
\text { Ksoil }_{i}=\left\{\begin{array}{l}
\frac{1}{\frac{T h T u b}{L a m T u b}+\frac{D l_{i} / 2}{L a m S o i l_{i}}} \text { if neighbor is soil } \\
\frac{1}{\frac{D l / 2}{L a m T u b}+\frac{D l_{i} / 2}{L a m T u b}} \text { if neighbor is tube }
\end{array}\right.
$$

- Heat from frictional losses relates to pressure drop along the tubes, which commonly writtes [5] as

$$
\Delta \text { PrAir }=\text { Rfric } \cdot \frac{D l}{\text { Dtub }} \cdot \frac{\text { RhoAir } \cdot \text { Vair }^{2}}{2}
$$

or

$$
\begin{equation*}
\Delta \text { PrAir }=\text { Rfric } \cdot \frac{\text { Dl } \cdot \text { RhoAir }}{2} \cdot \frac{\text { Fair }^{2}}{\text { Sair }^{2} \cdot \text { Dtub }} \tag{12}
\end{equation*}
$$

where the friction coefficient Rfric is here considered to be independent of air velocity, and the hydraulic diameter of the tube writes as

$$
\begin{equation*}
\text { Dtub }=\frac{4 \cdot \text { Sair }}{C t u b} \tag{13}
\end{equation*}
$$

Related energy rate then writes as

$$
\begin{equation*}
\text { Pfric }=\text { Fair } \cdot \Delta \text { PrAir } \tag{14}
\end{equation*}
$$

and is supposed to be gained entirely by the airflow (see energy balance further on).

- Heat lost by free water computes as

$$
\begin{equation*}
P_{w a t}=C m W a t \cdot \frac{M w a t_{t-1} \cdot\left(\text { Ttub }_{t-1}-T t u b\right)+M w a t I n \cdot\left(\text { Ttub }_{i \pm i}-T t u b\right)}{D t} \tag{15}
\end{equation*}
$$

- Internal heat gain is the heat gained by the tube :

$$
\begin{equation*}
\text { Pint }=\frac{C v T u b \cdot V o l T u b \cdot\left(T t u b-T t u b_{t-1}\right)}{D t} \tag{16}
\end{equation*}
$$

Preceding energy rates allow to calculate new tube temperature and free water content of actual node, as well as air temperature and humidity ratio of next node. Since the saturated humidity in (9) is non-linear in terms of temperature, Ttub is determined by numerical resolution of the tube energy balance

$$
\begin{equation*}
\text { Pint }=\text { Psbl }+ \text { Plat }+ \text { Psoil }+ \text { Pwat } \tag{17}
\end{equation*}
$$

while water balance readily yields

$$
\begin{equation*}
\text { Mwat }=M_{\text {wat }}^{t-1}+\text { MwatLat }+ \text { MwatInf }+ \text { MwatIn }- \text { MwatOut } . \tag{18}
\end{equation*}
$$

Sensible energy and water balance on air finaly yield air conditions of next node ( $i \pm 1$ ) :

$$
\begin{align*}
& \text { Tair }_{i \pm 1}=\text { Tair }+\frac{\text { Pfric }- \text { Psbl }}{(\text { CmAir }+ \text { Hrat } \cdot \text { CmVap }) \cdot \text { RhoAir } \cdot \text { Sair } \cdot \text { Vair }},  \tag{19}\\
& \text { Hrat }_{i \pm 1}=\text { Hrat }-\frac{\text { MwatLat }}{\text { RhoAir } \cdot \text { Sair } \cdot \text { Vair } \cdot \text { Dt }}, \tag{20}
\end{align*}
$$

where calculation can be pursued in same manner.
Soil-soil, soil-tube and soil-surface exchanges
Dynamic of soil nodes relies on diffusive heat from neighbor nodes :

$$
\begin{equation*}
\text { Psoil }=\sum_{i=1}^{6} \text { Ssoil }_{i} \cdot \operatorname{Ksoil}_{i}\left(T_{i}-\text { Tsoil }_{t-1}\right) \tag{21}
\end{equation*}
$$

where

$$
T_{i}= \begin{cases}T_{s o i l_{i, t-1}} & \text { if neighbor is soil } \\ T_{t u b_{i, t}} & \text { if neighbor is tube } \\ T s u r f_{i, t} & \text { if neighbor is surface }\end{cases}
$$

and

$$
\text { Ksoil }_{i}=\left\{\begin{array}{cc}
\frac{1}{\frac{D l / 2}{\text { LamSoil }}+\frac{D l_{i} / 2}{\text { LamSoil }}} & \text { if neighbor is soil } \\
\frac{1}{\frac{D l / 2}{\text { LamSoil }}+\frac{T h T u b}{\text { LamTub }}} & \text { if neighbor is tube } \\
\frac{1}{\frac{D l / 2}{\text { LamSoil }}+\text { Rsurf }} & \text { if neighbor is surface }
\end{array}\right.
$$

It allows to compute new soil temperature :

$$
\begin{equation*}
\text { Tsoil }=\text { Tsoil }_{t-1}+\frac{P_{\text {soil }}}{\text { CvSoil } \cdot \text { VolSoil }} . \tag{22}
\end{equation*}
$$

## Initialisation

Hypocaust is initialised with a common initial temperature for all nodes, as well as a common initial water thickness along all tubes. Optionaly one may define additional initial temperatures and water thicknesses for certain nodes or node clusters (see further on, definition of parameter file).

## TRNSYS Component Configuration

Source code is separated into two files :

- Type61.for contains actual routine and is organised in different subroutines.
- Type61.inc is an include file used by the subroutines. It contains definition of variables and their organisation in common blocks, as well as definition of maximum allowed sizes, which are listed hereafter with their default values :

| NIMax | max number of nodes along x | 40 |  |
| :--- | :--- | ---: | :--- |
| NJMax | max number of nodes along y (per module) | $\left.100^{1}\right)$ |  |
| NKMax | max number of nodes along Z (per module) | $20^{1}$ |  |
| NtubMax | max number of tubes (per module) | $\left.20^{1}\right)$ |  |
| NsoilMax | max number of soiltypes | 10 |  |
| NsurfMax | max number of surfaces | $\left.6^{2}\right)$ |  |
| NoptMax | max number of optional outputs | $100^{2)}$ |  |
| NiniMax | max number of initialisation conditions | 20 |  |

1) module $=$ relevant part in $y-z$ plane (see further up, description of geometry).
2) Changing default values for maximum number of surfaces or maximum number of optional outputs will need renumeration of routine arguments (parameters, inputs and outputs) as defined in information flow diagram.

Input data is separated into three groups, of which two are passed as arguments, the last one read from a file :

- Parameters describe fixed data that deal with linking to other modules and with simulation deck.
- Inputs describe variable data.
- Parameters which are proper to the model are passed by means of a Parameter definition file, which is read by the routine at initialisation. While reading, the data is checked and rewritten to a control file (see below), so that eventual errors can be tracked.

Output data is separated into two groups, of which first one is returned as argument, second one written to a file :

- Outputs describe variable data, which can be linked to other modules.
- Parameters which are derived from supplied parameter file or from simulation deck are written to a Parameter control file, which can be used to check for proper definition. As pointed out, first part of this file is a formatted and commented copy of Parameter definition file (which it can substitute).

A synoptic view of these data groups is to be found in the information flow diagarm (next section), while this section presents each of them in a detailed table (with explanatory notes following last table).

Note, especially in case of debugging, that data is passed to/from the routine with TRNSYS compatible units as defined hereafter, where it is converted to standard SI units.

Parameters

| Number | Symbol | Definition and unit |  |
| :--- | :--- | :--- | :--- |
| 1 | IparDef | Logical unit of Parameter definition file $[-]$ | 1) |
| 2 | IparCon | Logical unit of Parameter control file $[-]$ | 1) |
| 3 | Dt | Internal timestep $[\mathrm{hr}]$ | $2)$ |
| 4 | FairMin | Minimum airflow $\left[\mathrm{m}^{3} / \mathrm{hr}\right]$ | $3)$ |
| 5 | DTtubTol | Temperature tolerance for tube energy balance $[\mathrm{K}]$ | $4)$ |
| $6-11$ | TypSurf | Linking modes for surfaces $1-6[-]$ | S) |
| $12-17$ | Rsurf | Heat resistance at surfaces $1-6[\mathrm{~K} \mathrm{~m} 2 \mathrm{hr} / \mathrm{kJ}]$ |  |

Inputs

| Number | Symbol | Definition and unit |  |
| :--- | :--- | :--- | :--- |
| 1 | FairTot | Airflow, total over all modules $[\mathrm{m} 3 / \mathrm{hr}]$ | 6) |
| 2 | TairIn | Inlet temperature $[\mathrm{degC}]$ |  |
| 3 | HrelIn | Inlet relative humidity [pcent $]$ |  |
| 4 | PrAir | Air pressure [bar] | 7) |
| 5 | FwatInfTot | Water infiltration, total over all modules $[\mathrm{m} 3 / \mathrm{hr}]$ | $8)$ |
| $6-11$ | Xsurf | Surface conditions for surfaces 1-6[degC] or $[\mathrm{kJ} / \mathrm{hr}]$ | $5)$ |

## Parameter definition file

Each data set hereafter is written on one line (exception for TypSoil arrays, which take NK or $N K+2$ lines). Data within one dataset is separated by commas or blanks. Comments can be entered by using an asterix ( ${ }^{*}$ ) in first column.

## Symbol

Nmod,Nsec,Nsoil,Nsurf,NI,NJ, NK
Dx (1:NI)
Dy (1:NJ)
Dz (1:NK)
TypSec(1:NI)
TypSoil (1:NJ,1:NK)
TypSoil ( $0: N J+1,0: N K+1$ )

## Definition and unit

Number of : modules, cross-sections, surfaces, nodes along x -axis, nodes along y -axis, nodes along z -axis [-]
Node width along x -axis [m]
Node width along y-axis [m]
Node width along z-axis [m]
Type of used cross-sections along $x$-axis [-]
Type of surfaces on frontal cross-section [-]
Type of soils/surfaces for typical cross-section in y-z ${ }^{12)}$ plane [-]

| TypSoil (1:NJ,1:NK) | Type of surfaces on rear cross-section [-] 11) |
| :---: | :---: |
| PosInf | Position of water infiltration [-] 8) |
| Kair0, Kair1 | Air-tube exchange coefficients 13) |
|  | [ $\mathrm{kJ} / \mathrm{hr} \mathrm{K} \mathrm{m} 2]$ and [( $\mathrm{kJ} / \mathrm{hr} \mathrm{K} \mathrm{m} 2) /(\mathrm{m} / \mathrm{s})$ ] |
| LamSoil, CvSoil | Soil conductivity [ $\mathrm{kJ} / \mathrm{hr} \mathrm{K} \mathrm{m}]$ and capacity [ $\mathrm{kJ} / \mathrm{K} \mathrm{m} 3]$ 14) |
| LamTub, CvTub | Tube conductivity [ $\mathrm{kJ} / \mathrm{hr} \mathrm{K} \mathrm{m}]$ and capacity $[\mathrm{kJ} / \mathrm{K} \mathrm{m} 3]$ |
| ThTub, CtubCor, Rfric | Tube thickness [m], circumference correction factor $[-] \quad 9)$ and friction coefficient [-] |
| TypWatFlow (-1:1) | Type of water flow [-] 16) |
| Vwat (-1:1) | Velocity of water flow [m/hr] 16) |
| NiniSoil, NiniWat | Number of initial conditions (soil temperatures and waterthicknesses) [-] |
| TiniSoil, PosIniSoil (1:6) | Initial temperature [degC] and corresponding node position [-] |
| ThIniWat, PosIniWat (1:6) | Initial waterthickness $[\mathrm{m}]$ and corresponding node position [-] |
| Nopt | Number of optional outputs 20) |
| TypOpt, PosOpt (1:6) | Type of optional output [-] and corresponding node position [-] |
| utputs |  |
| Number Symbol | Definition and unit |
| 1 TairOut | Outlet temperature [ $\operatorname{deg} \mathrm{C}]$ |
| 2 HrelOut | Outlet relative humidity [pcent] |
| 3 PsblTot | Sensible energy rate lost by airflow, total over tubes and modules [ $\mathrm{kJ} / \mathrm{hr}$ ] |
| 4 PlatTot | Latent energy rate lost by airflow, total over tubes and modules [ $\mathrm{kJ} / \mathrm{hr}$ ] |
| 5-10 Xbord | Equivalent border output for surfaces 1-6 [ degC ] or [kJ/hr] |
| 11-20 Xopt | Optional outputs 20) |

Parameter control file
Data hereafter is written at end of file, after formatted copy of Parameter definition file.

Symbol<br>Ntub<br>IflowIni<br>IflowEnd<br>PosTub(1:2)<br>Lx<br>Ly<br>Lz<br>Ltub<br>SairTot

StubTot

## Definition and unit

Number of tubes (per module) [-]
Node index of tube start along $x$-axis [-]
Node index of tube end along $x$-axis [-]
Node index of tube position along $y$ - and $z$-axis [-]
Length of hypocaust [m]
Width of hypocaust (total over modules) [ m ]
Depth of hypocaust [m]
Length of tubes [m]
Tube cross-section area (total over all tubes and modules) [m2]
Tube surface (total over all tubes and modules) [m2]

| ZairTot | Normalisation factor for airflow distribution $[\mathrm{m} 5 / 2]$ |  |
| :--- | :--- | :--- |
| SinfTot | Water infiltration surface, total over all modules $[\mathrm{m} 2]$ | $8)$ |
| Sbord | Border area (total over all modules) $[\mathrm{m} 2]$ |  |
| Kbord | Equivalent border conduction coefficient $[\mathrm{kJ} / \mathrm{hr} \mathrm{K} \mathrm{m} 2]$ |  |
| DtSoil | Maximum internal timestep for stability of soil |  |
|  | temperature [hr] |  |
| DtWat | Maximum internal timestep for consistency of water |  |
|  | flow [hr] |  |
| FairMinTub | Minimum air flow for stability of air temperature |  |
|  | $[\mathrm{m} 3 / \mathrm{hr}]$ |  |
| Dt | Internal timestep effectively used in simulation $[\mathrm{hr}]$ |  |
| FairMin | Minimum air effectively flow used in simulation |  |
|  | $[\mathrm{m} 3 / \mathrm{hr}]$ |  |

## Explanatory notes for preceeding tables

1) Unless assigned in simulation deck with user-defined name, parameter definition and control files must by default be named ParamDef.txt and ParamCon.txt.
2) Since calculation of soil temperature is of explicit type, internal timestep should not exceed a maximum theoretical value DtSoil, which is proportional to smallest node volume of soil (problem of temperature oscillation). Consistency of water flow calculation (equation 3) also implies a maximum value DtWat for internal timestep, proportional to shortest tube node. Both of these computed values are written to the parameter control file. Type 61 usualy takes the smallest of these two values for the internal timestep (which happens by setting the $3^{\text {rd }}$ routine parameter $D t$ to zero). The user may alternatively control soil temperature oscillation by defining a larger or smaller internal timestep himself (which happens by setting the $3^{\text {rd }}$ routine parameter $D t$ to a positive value), in which case the value $D t$ Wat should not be exceeded though.
3) So as to avoid oscillations of air temperature along the tube, airflow should not exceed a theoretical minimum value FairMinTub, which is written to the parameter control file. Type 61 usualy takes this value as a lower limit to the airflow (which happens by setting the $4^{\text {th }}$ routine parameter FairMin to zero). The user may alternatively control air temperature oscillation by defining a larger or smaller minimum airflow himself (which happens by setting the $4^{\text {th }}$ routine parameter FairMin to a positive value). In both cases an airflow smaller than the minmum value will be set to zero (no air-tube exchange, only diffusion within soil).
4) Temperature tolerance $(>0)$ sets precision of numerical resolution of energy balance in tube (equation 17).
5) For each surface, linking mode is one of the following :

0 : corresponding input Xsurf is surface temperature, output Xbord is inflowing energy rate.
1 : corresponding input Xsurf is is inflowing energy rate, output Xbord is equivalent border temperature.
6) Airflow direction along $x$-axis is carried by sign of airflow. If airflow is smaller (in absolute value) than minimum airflow FairMin (see parameter control file) it is considered as zero (no air-tube exchange, only diffusion within soil).
7) Air pressure is used to convert volume flow in mass flow as well as to determine humidity ratio from relative humidity (equation 9). In usual cases its dynamic is not known and it is suggested to take standard atmosferic pressure at local altitude, which can be approximated by :

$$
\text { PrAir }=\text { PrAir }_{0} \exp \left(-h / h_{0}\right) \text { with } \text { PrAir }_{0}=1.01325 \text { bar, } h_{0}=7656 \mathrm{~m} .
$$

8) Water infiltration is distributed on a certain tube area SinfTot, defined by the rectangular node cluster Posinf on which infiltration is to take place.
PosInf(1) and PosInf(4) are lower and upper node index along x-axis.
PosInf(2) and PosInf(5) are lower and upper node index along y-axis.
$\operatorname{Posinf}(3)$ and $\operatorname{Posinf}(6)$ are lower and upper node index along $z$-axis.
Only tube nodes within this cluster are considered for water infiltration.
9) Even for non-rectangular tubes, node width must be chosen so that cross-section area is given by $D y D z$. Cross-section perimetrer, exchange surfaces and hydraulic diameter will be corrected by tube circumference correction factor CtubCor. Latter is defined as the ratio between real tube perimeter and rectangular tube perimeter $2(D y+D z)$. For circular tubes node width has to be chosen so that $D y=D z=r \sqrt{\pi} \cong 1.772 r$ and circumference correction factor becomes $1 / 2 \sqrt{\pi} \cong 0.8862$. In case of a symetry plane passing in the middle of some tubes (tube node at hypocaust border, with latteral adiabatic condition) one furthermore has to divide Dy by half.
Generally speaking node widths $D x, D y$ and $D z$ have to be chosen according to given problem, reminding that small soil volumes will lead to small internal timesteps and increase of runtime. Tube thickness $T h T u b$ may however be set to zero.
10) TypSec (I:NI) are positive integer numbers which refer to further on defined typical crosssections along x -axis.
11) TypSoil ( $1: N J, 1: N K$ ) are integer numbers which refer to given surface conditions for front and rear of hypocaust module (see example at end).
12) TypSoil ( $0: N J+1,0: N K+1)$ are integer numbers which refer to further on defined soil types (bulk) or to given surface conditions (border). Exception are the 4 corners TypSoil ( 0,0 ), TypSoil $(N J+1,0)$, TypSoil $(0, N K+1)$, TypSoil $(N J+1, N K+1)$ which have no significance and are not defined (see figure 1 and example at end). This data set has to be repeated for the Nsec number of typical cross-sections.
13) Common values for air-tube exchange coefficients [3] are :

Kair0:7-11[kJ/hr Km2]
Kairl: 14-18[(kJ/hr K m2)/(m/s)]
14) This line has to be repeated for the Nsoil number of soils.
15) Typical values for Friction coefficient are $0.01-0.02$ [-].
16) Specification of water flow is given for all 3 airflow diections (negative, zero, positive). TypWatFlow indicates whether free water is to flow along the tubes $(=1)$ or to be ejected out $(=2)$. Vwat $(\geq 0)$ specifies velocity of waterflow (if TypWatFlow $=1$ ).
17) Initial temperatures are given for rectangular node clusters, defined by PosIniSoil :

PosIniSoil( 1 ) and PosIniSoil(4) are lower and upper node index along $x$-axis,
PosIniSoil(2) and PosIniSoil(5) are lower and upper node index along y-axis,
PosIniSoil(3) and PosIniSoil(6) are lower and upper node index along z-axis,
except for first initial temperature which is applied to all nodes and thus does not need definition of PosIniSoil (see example at end).
Same structure accounts for initial water thicknesses. In this case only those nodes within the cluster which do effectively corespond to tube nodes are taken into account though.
18) This line is repeated for the $N t u b$ number of tubes.
19) This line is repeated for the Nsurf number of surfaces.
20) Nopt defines the number of desired optional outputs. For each one of them TypOpt specifies the type of optional output and takes a value from one of the three following tables. PosOpt finally defines the rectangular node cluster for which the optional output is to be considered : PosOpt(1) and PosOpt(4) are lower and upper node index along x-axis, PosOpt(2) and PosOpt(5) are lower and upper node index along y-axis, $\operatorname{PosOpt}(3)$ and $\operatorname{PosOpt}(6)$ are lower and upper node index along z-axis. If TypOpt relates to tube/air nodes, only tube nodes within cluster will be considered. If TypOpt relates to soil nodes, only soil nodes within cluster will be considered.
If TypOpt relates to miscelanous data, PosOpt is of no significance and should be set to 1 .
Optional outputs for tube nodes :

| Type | Symbol | Definition and unit |  |
| :---: | :---: | :---: | :---: |
| 1 | Tair | Air temperature [degC] | * |
| 2 | Hrel | Air relative humidity [pcent] | * |
| 3 | Habs | Air absolute humidity [bar] | * |
| 4 | Hrat | Air humidity ratio [ kg vapor/kg air] | * |
| 5 | Mwat | Free water in node [m3] | ** |
| 6 | MwatLat/Dt | Water condensing ( $>0$ ) or evaporating ( $<0$ ) [m3/hr] | ** |
| 7 | MwatIn/Dt | Water flowing into node [m3/hr] | ** |
| 8 | MwatInfiDt | Water infiltrating into node [ $\mathrm{m} 3 / \mathrm{hr}$ ] | ** |
| 9 | MwatOut/Dt | Water flowing out of node [ $\mathrm{m} 3 / \mathrm{hr}$ ] | ** |
| 10 | Tsoil | Tube temperature [degC] | ** |
| 11 | Psbl | Sensible energy rate from air to tube [ $\mathrm{kJ} / \mathrm{hr}$ ] | ** |
| 12 | Plat | Latent energy rate from air to tube [ $\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 13 | Pwat | Energy rate lost by free water [ $\mathrm{kJ} / \mathrm{hr}$ ] | ** |
| 14 | Pfric | Energy rate from frictional losses [ $\mathrm{kJ} / \mathrm{hr}$ ] |  |
| 15 | Psoil(0) | Energy rate diffused from all 6 neighbor nodes [ $\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 16 | Psoil(1) | Energy rate diffused from previous neighbor node along x -axis (from surface if border node) $[\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 17 | Psoil(2) | Energy rate diffused from next neighbor node along $x$ axis (from surface if border node) $[\mathrm{kJ} / \mathrm{hr}]$ | * |
| 18 | Psoil(3) | Energy rate diffused from previous neighbor node along y-axis (from surface if border node) [ $\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 19 | Psoil(4) | Energy rate diffused from next neighbor node along yaxis (from surface if border node) $[\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 20 | Psoil(5) | Energy rate diffused from previous neighbor node along z -axis (from surface if border node) [ $\mathrm{kJ} / \mathrm{hr}$ ] | ** |
| 21 | Psoil(6) | Energy rate diffused from next neighbor node along zaxis (from surface if border node) $[\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 22 | Pint | Energy rate of internal gains [ $\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 23 | Fair | Air flowrate [m3/hr] | * |
| 24 | Vair | Air velocity [m/s] | * |

Optional outputs for soil nodes:

| Type | Symbol | Definition and unit |  |
| :---: | :---: | :---: | :---: |
| 101 | Tsoil | Soil temperature [degC] | * |
| 102 | Psoil(0) | Energy rate diffused from all 6 neighbor nodes [ $\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 103 | Psoil(1) | Energy rate diffused from previous neighbor node along x -axis (from surface if border node) [ $\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 104 | Psoil(2) | Energy rate diffused from next neighbor node along xaxis (from surface if border node) $[\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 105 | Psoil(3) | Energy rate diffused from previous neighbor node along y-axis (from surface if border node) [ $\mathrm{kJ} / \mathrm{hr}$ ] | ** |
| 106 | Psoil(4) | Energy rate diffused from next neighbor node along yaxis (from surface if border node) $[\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 107 | Psoil(5) | Energy rate diffused from previous neighbor node along z -axis (from surface if border node) [ $\mathrm{kJ} / \mathrm{hr}$ ] | ** |
| 108 | Psoil(6) | Energy rate diffused from next neighbor node along zaxis (from surface if border node) $[\mathrm{kJ} / \mathrm{hr}]$ | ** |
| 109 | Pint | Energy rate of internal gains [ $\mathrm{kJ} / \mathrm{hr}$ ] | ** |

* averaged over node cluster
** integrated over node cluster and multiplied by number of modules
Miscellaneous data for optional output :

| Type | Symbol <br> 201 | Definition and unit <br> Potal inflowing energy rate through surfaces (over all <br> modules) [kJ/hr] |
| :--- | :--- | :--- |
| 202 | PwatTot | Total energy loss of free water (over all modules) <br> $[\mathrm{kJ} / \mathrm{hr}]$ |
| 203 | PfricTot | Total frictional losses (over all modules) $[\mathrm{kJ} / \mathrm{hr}]$ <br> 204 |
| PintTot |  |  |
| $[\mathrm{kJ} / \mathrm{hr}]$ |  |  |

## Références

1. Hollmuller P., Lachal B., TRNSYS compatible moist air hypocaust model : description and validation, Centre universitaire d'études des problèmes de l'énergie, CH - 1205 Genève, 1998.
2. Razafinjohany E., Etude comparative dans les serres agricoles de deux systèmes de stockage de la chaleur influencé de l'humidité de l'air, Thèse, 1989, Académie de Montpelier, Université de Perpignan.
3. Molineaux B., Lachal B., and Guisan O., Thermal analysis of five outdoor swimming pools heated by unglazed solar collectors, Solar Energy, Vol. 53, Nb. 1, July 1994, pp. 21-26.
4. Incropera F. P., De Witt D. P., Fundamentals of heat and mass transfer, John Wiley \& Sons Inc., 1990.
5. 1989 Ashrae Handbook, Fundamentals, American society of heating, refrigerating and air conditioning engineers inc., 1791 Tullie Circle, N.E., Atlanta, GA 30329.

## Information Flow Diagram



## Example

## Description

Example is the underground cooling system shown in Fig. 1. It is a mere case study ment to show the possibility of linking Type61 to the multizone building Type 56 and to check consistency of exchanged energy rates as well as of other internal variables. Hence following hypothesis are made :

- Ambient conditions are constant : temperature of $30^{\circ} \mathrm{C}$, humidity of $50 \%$, no solar radiation.
- Building is simplified to its uttermost : a first zone ( $8 \mathrm{~m} 2,16 \mathrm{~m} 3$ ) with simple brick wall is free-floating and adjoins a second zone ( $12 \mathrm{~m} 2,39 \mathrm{~m} 3$ ) with insulated brick wall and at fixed temperature $\left(15^{\circ} \mathrm{C}\right)$. No windows are taken into account and no infiltration nor crossventilation is considered.
- Pipe system is underneath building and latteraly not insulated, wherefor lateral and from hypocaust distinct soil is taken into account.
- Airflow is constant ( $1000 \mathrm{~m}^{3} / \mathrm{hr}$ ) and is not injected into building but supposed to be used elsewhere.
- No water infiltration is considered, nor does free water flow along the tubes.
- Initial temperatures are $10^{\circ} \mathrm{C}$ for hypocaust, $15^{\circ} \mathrm{C}$ for surrounding soil and building.

Following variables are defined and analysed (some of which, for checking of proper energy and mass balance, are calculated by two alternative ways defined in the deck) :

| Psbl | : senible energy lost by airflow |
| :--- | :--- |
| Plat | : latent energy lost by airflow |
| Pin | : internal gains of hypocaust and surrounding soil |
| PinG, PinG\# | : internal gains of surrounding soil |
| PinH, PinH\# | : internal gains of hypocaust |
| PinHt | : internal gains of hypocaust tubes |
| PinHs | : internal gains of hypocaust soil |
| Pfree, Pfree\# | : energy diffused from free-floating zone into hypocaust |
| Pfix, Pfix\# | : energy diffused from fixed setpoint zone into hypocaust |
| Pamb | : energy diffused from ambient into surrounding soil |
| Pfront | : energy diffused from surrounding soil front of the building into hypocaust |
| Pback | : energy diffused from surrounding soil back of the building into hypocaust |
| Pside | : energy diffused from surrounding soil to side of the building into hypocaust |
| Pwat | : energy diffused from free water into hypocaust |
| Pfric | : friction losses |
| T1-T4 | : temperatures of airflow along tubes (mean value of all tubes) |
| Tout | : temperature of airflow at outlet |
| Tfree | : temperature of free-floating zone, air |
| TgFree | : temperature of free-floating zone, ground |
| Tfix | : temperature of fixed setpoint zone, air |
| TgFree | : temperature of fixed setpoint zone, ground |
| Mwat, Mwat\# | : free water within tubes |
| dMlat | : condensation/evaporation within tubes |
| dMout | : total outflowing water. |

Next pages show files for parametrisation of the system (parameter definition file for Type 61, building definition file for Type 56 , simulation deck), after which corresponding simulation results are discussed.

Type61.par: parameter definition file (Type 61)


| 0 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 2 | 2 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 0 |
| 0 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| * Typsoil | for | sec\# | 3 | (through | setpoint-zone only) | $[-]:$ |  |  |  |  |  |  |  |
| 0 | 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |  |
| 0 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |  |
| 0 | 2 | 2 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 0 |
| 0 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
| 0 | 2 | 2 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 1 | 1 | 0 |
| 0 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
| 0 | 2 | 2 | 1 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 1 | 0 | 0 |
|  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |

* TypSoil for rear surface [-]:

| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

* Posinf [-]:
$\begin{array}{llllll}1 & 1 & 1 & 9 & 12 & 7\end{array}$
* Kairo [kJ/K m2] , Kairi [(kJ/K m2)/(m/s)]:
$0.1800 \mathrm{E}+02 \quad 0.1400 \mathrm{E}+02$
* LamSoil [kJ/K m], CvSoil [kJ/K m3]:
$0.7200 \mathrm{E}+01 \quad 0.1000 \mathrm{E}+04$
$0.5400 \mathrm{E}+01 \quad 0.1000 \mathrm{E}+04$
* LamTub [kJ/K m], CvTub [kJ/K m3]:
$0.7200 \mathrm{E}+01 \quad 0.1000 \mathrm{E}+04$
* ThTub [m], CtubCor [-], Cfric [-]:
5.0000E-03 0.8862E+00 2.0000E-02
* TypWatFlow [-], Vwat [m/h]:
111
$0.0000 \mathrm{E}+00 \quad 0.0000 \mathrm{E}+00 \quad 0.0000 \mathrm{E}+00$
* NiniSoil,NiniWat [-]:
21
* TiniSoil [degC], PosIniSoil [-]:
$0.1500 \mathrm{E}+02$
$\begin{array}{lllllll}0.1000 E+02 & 3 & 3 & 1 & 11 & 12 & 7\end{array}$
* ThIniWat [m], posIniWat [-]:
$0.0000 \mathrm{E}+00$
* Nopt [-]:
17

| $*$ Typopt | $[-]$, | PosOpt $[-]:$ |  |  |  |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | :--- | :--- |
| 107 | 3 | 3 | 1 | 5 | 12 | 1 | !Pfree\# |
| 107 | 6 | 3 | 1 | 11 | 12 | 1 | !Pfix\# |
| 103 | 3 | 3 | 1 | 3 | 12 | 7 | !Pfront |
| 104 | 11 | 3 | 1 | 11 | 12 | 7 | !Pback |
| 105 | 3 | 3 | 1 | 11 | 3 | 7 | !Pside |
| 202 | 1 | 1 | 1 | 1 | 1 | 1 | !Pwat |
| 203 | 1 | 1 | 1 | 1 | 1 | 1 | !Pfric |
| 204 | 1 | 1 | 1 | 1 | 1 | 1 | !Pin |
| 22 | 3 | 3 | 1 | 11 | 12 | 7 | !PinHt |
| 109 | 3 | 3 | 1 | 11 | 12 | 7 | !PinHs |
| 5 | 3 | 3 | 1 | 11 | 12 | 7 | !Mwat |
| 6 | 3 | 3 | 1 | 11 | 12 | 7 | !dM1at |
| 9 | 11 | 3 | 1 | 11 | 12 | 7 | !dMout |
| 1 | 4 | 3 | 1 | 4 | 12 | 7 | !T1 |
| 1 | 6 | 3 | 1 | 6 | 12 | 7 | !T2 |
| 1 | 8 | 3 | 1 | 8 | 12 | 7 | !T3 |
| 1 | 10 | 3 | 1 | 10 | 12 | 7 | !T4 |
| $* * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * * *$ |  |  |  |  |  |  |  |

## Observations :

- Because of symetry in the y-z plane, only half of the hypocaust has to be simulated, cutting middle two pipes by half ( $\operatorname{Nmod}=2$ and last node width $D y$ is half the width of other ones).
3 cross-sections must be defined, one outside the building, two through the building (one cutting both zones, the other one through fixed zone only), as well as 3 surface conditions (ambient and floor of both zones).
- 2 temperature initialisation are used, for soils surrounding and beneath building respectively.

Building.bui : building definition file (Type 56)

```
************************************************************************
* TYPE 56 DESCRIPTION
    *
************************************************************************
PROPERTIES
************************************************************************
DENSTTY=1.204 : CAPACITY=1.012 : HVAPOR=2454: SIGMA=2.041E-07
RTEMP =293.15
TYPES
************************************************************************
*-- LAYERS
LAYER Brick30
THICKNESS=.30 : CONDUCTTVITY=3 : CAPACITY=1 : DENSITY=1800
LAYER Insul10
THICKNESS=.10 : CONDUCTTVITY=0.144 : CAPACITY=0.72 : DENSITY=90
LAYER SOil40
THICKNESS =.40 : CONDUCTTVITY=7.2 : CAPACITY=1 : DENSTTY=1000
* - INPUTS
INPUTS TgFree TgFix
```

```
*-- WALLS
WALL Brick
LAYERS Brick30
ABS-FRONT=. }8\mathrm{ : ABS-BACK=. }8\mathrm{ : HFRONT=15 : HBACK=15
WALL Insul_Brick
LAYERS Insul10 Brick30
ABS-FRONT=. }8\mathrm{ : ABS-BACK=.8 : HFRON'=15 : HBACK=15
WALL Soil
LAYERS SOil40
ABS-FRONT=.8 : ABS-BACK=0 : HFRONT=15 : HBACK=36
* rem : HBACK must be equal to Kbord from Type 61 *
WALL Insul_Soil
LAYERS Insul10 Soil40
ABS-FRONT=.8 : ABS-BACK=0 : HFRONT=15 : HBACK=36
* rem : HBACK must be equal to Kbord from Type 61 *
*-- COOLING
COOLING COOlFix
ON=15 : POWER=1E6 : HUMIDITY=0
*-- ORIENTATIONS
ORIENTATIONS Ambient
*-- ZONES
ZONES Free Fix
BUILDING
********************************************************************************
*-- ZONE Free
ZONE Free
WALL=Insul_Brick : AREA=16 : ADJACENT=Fix : BACK : COUPLING=0
WALE=Brick : AREA=16 : EXTERNAL : ORIENTATION=Ambient : FSKY=0.5
WALL=Soil : AREA=8 : BOUNDARY=INPUT TgFree : COUPLING=0
REGIME
CAPACITANCE=1E+3 : VOLUME=16 : TINITIAL=15 : PHIINITIAL=50.0 : WCAPR=1
*.-- ZONE Fix
ZONE Fix
WALL=Insul Brick : AREA=16 : ADJACENTmFree : FRONT : COUPLING=0
WALE=Insul_Brick : AREA=41 : EXTERNAL : ORIENTATTON=Ambient : FSKY=0.5
WALE=Insul_SOil : AREA=12 : BOUNDARY=INPUT TgFix : COUPLING=0
REGIME
COOL=COOlFix
CAPACITANCE=1E+3 : VOLUME=39 : TINITIAL=15 : PHTINTTIAL=50.0 : WCAPR=1
OUTPUTS
***************************************************************************
*-- TRANSFER
TRANSFER : TIMEBASE=1
```

```
*-- OUTPuts
ZONES=Free
NTYPES=1 20
ZONES=Fix
NTYPES=1 20
END
*****************************************************************************
```


## Observations :

- Preceding file must be processed by BID program before it can be used by Type 56 (for more details refer to Type56 component description).
- Note that for proper coupling with Type $61 H B A C K$ of soil is set to identical value as $K b o r d$ from hypocaust and ground areas are identical to Ssurf from hypocaust (see Parameter control file to check this).


## Type61.dck: simulation deck file

```
***************************************************************
* SIMULATION:
***************************************************************
```



```
    ASSIGN Trnsys.txt 6
    ASSIGN Out1.txt 101
    ASSIGN Out2.txt 102
    ASSIGN Out3.txt 103
    ASSIGN Type61.par 200
    ASSIGN Type61.con 201
    ASSIGN Building.bld 300
    A.SSIGN Building.trn 301
    ASSIGN Building.win 302
```




```
    EQUATTONS 37
*-m...-------......------
    Dtsim =1
    Tamb = 30
    Hamb = 50
    Aflow = 1000
*-----------..-------------
    Tfree = [1, 1]
    Tfix = [1,5]
    Pfree = - [1,4]
    Pfix = - [1,8]
*------.------...---------
    Tout = = [2,1]
    Psbl=[2,3]
    Plat = [2,4]
    TgFree = [2,5]
    TgFix=[2,6]
```

```
    Pamb = [2,7]
    Pfree# = [2,11]
    Pfix# = [2,12]
    pfront = [2,13]
    Pback = [2,14]
    Pside = [2,15]
    Pwat = [2,16]
    Pfric = [2,17]
    Pin = [2,18]
    PinHt = [2,19]
    PinHs}=[2,20
    Mwat = = 2,21]*1000
    dMlat = [2,22]*1000
    dMout = [2,23]*1000
    T1=[2,24]
    T2 = [2,25]
    T3 = [2,26]
    T4 = [2,27]
*---------------------
    PinH = PinHt+PinHs
    Ping = Pin-PinHt-PinHs
    PinH# = Psbl+Plat+Pfree+Pfix+Pfront+Pback+Pside+Pwat
    PinG# = Pamb-Pfront-Pback-Pside
    dMwat = dMlat-dMout
    Mwat# = GT(TIME,1)*[3,1]+LT(TTMME, 2)*dMwat
* Mwat# = [3,1] replaced by preceding line because of bug in
* integrator Type55
```




```
    SIMULATION 1 100 DtSim
    TOLERANCES -0.0001 -0.0001
```



```
***********************************************************************
* COMPONENTS:
**********************************************************************
```



```
* Multizone Building
*----------------w-----------------------------------------------------------
UNIT 1 TYPE 56
PARAMETERS 5
*---------------------
* 01) Logical unit of building description file
* 02) Logical unit of transfer coefficient file
* 03) Logical unit of window library file
* 04) Mode of calculation for star network
* 05) Weighting factor for operative romm temperature
    300 301 302 0 0.5
INPUTS 8
*-----------------.----
* 01) Ambient temperature [degC]
* 02) Ambient humidity ratio [kg water / kg air]
* 03) Fictive sky temperature [degc]
```

```
* 04) Incident radiation for orientation ambient [kJ/hr]
* 05) Incident beam radiation for orientation ambient [kJ/hr]
* 06) Incident angle for orientation ambient [deg]
* 07) Ground temperature zone "Free" [deg C]
* 08) Ground temperature zone "Fix" [deg C]
\begin{tabular}{lllll} 
Tamb & 0,0 & Tamb & 0,0 & 0,0 \\
0,0 & TgFree & TgFix & & \\
\(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) \\
\(0.000 \mathrm{E}+00\) & \(0.100 \mathrm{E}+02\) & \(0.100 \mathrm{E}+02\) & &
\end{tabular}
* OUPUTS 8
*--..--....-.-----------.--
* 01) Temperature of zone "Free" [degC]
* 02) Energy rate from zone "Free" to zone "Fix" [kJ/hr]
* 03) Energy rate from zone "Free" to "Ambient" [kJ/hr]
* 04) Energy rate from zone "Free" to "Ground" [kJ/hr]
* 05) Temperature of zone "Fix" [degC]
* 06) Energy rate from zone "Fix" to zone "Free" [kJ/hr]
* 07) Energy rate from zone "Fix" to "Ambient" [kJ/hr]
* 08) Energy rate from zone "Fix" to "Ground" [kJ/hr]
```




```
* Hypocaust
UNIT 2 TYPE 61
PARAMETERS 17
*----------------..---
* 01) Logical unit parameter definition file
* 02) Logical unit parameter control file
* 03) Internal timestep [hr]
* 04) Minimum airflow [m3/hr]
* 05) Tolerance on tube temperature [K]
* 06-11) Surface types
* 12-17) Resistance at surface [K m2 hr/kJ]
\begin{tabular}{lllll}
\(2.000 \mathrm{E}+02\) & \(2.010 \mathrm{E}+02\) & \(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(1.000 \mathrm{E}-02\) \\
\(1.000 \mathrm{E}+00\) & \(1.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) \\
\(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(0.150 \mathrm{E}-01\) & \(0.000 \mathrm{E}+00\)
\end{tabular}
0.000E+00
INPUTS 11
*------------------.--
* 01) Air flow [m3/h]
* 02) Air inlet temperature [degc]
* 03) Air inlet humidity [pcent]
* 04) Air pressure [Pa]
* 05) Water infiltration [m3/h]
* 06-11) Surface conditions [degC or W]
\begin{tabular}{lllll} 
Aflow & Tamb & Hamb & 0,0 & 0,0 \\
Pfree & Pfix & Tamb & 0,0 & 0,0 \\
0.0 & & & & \\
\(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}+00\) & \(1.000 \mathrm{E}+00\) & \(0.000 \mathrm{E}-03\)
\end{tabular}
```

```
    0.000E+00 0.000E+00 Tamb 0.000E+00 0.000E+00
    0.000E+00
* OUPUTS 30
*-------------------------
* 01) Temperature of aix outlet [degc]
* 02) Humidity of air outlet [pcent]
* 03) Sensible energy rate delivered to ground [kJ/hr]
* 04) Latent energy rate delivered to ground [kJ/hr]
* 05-10) Equivalent border conditions [degC or kJ/hr]
* 11-30) Optional outputs [fct of output type]
```




```
* Integrator
```



```
    UNIT 3 TYPE 55
    PARAMETERS 7
    1 1 1 1 1 1E5 1 1E5
    INPUTS 1
    dMwat
    O
```




```
* Printers
```



```
* PARAMETERS
*------------...------------
* 01) Print time interval (>0mhours <0=months)
* 02) Time for start of printer (>0=hours <0=months)
* 03) Time for stop of printer (>0=hours <0mmonths)
* 04) Logical unit (<=0 For std Line Printer)
* Printer 1
    UNIT 11 TYPE 25
```



```
    PARAMETERS 4
    1.000E+00 0.000E+00 1.000E+05 1.010E+02
    INPUTS 10
    Psbl Plat Pfree Pfix Pamb
    Pfront Pback Pside Pwat Pfric
    Psbl Plat Pfree Pfix Pamb
    pfront Pback Pside Pwat Pfric
* Printer 2
    UNIT 12 TYPE 25
*--------...-----------...---
    PARAMETERS 4
    1.000E+00 0.000E+00 1.000E+05 1.020E+02
    INPUTS 10
    PinH PinG PinH# PinG# PEree#
    Pfix# Mwat Mwat# dMlat dMout
    PinH Ping PinH# PinG# PEree#
    Pfix# Mwat Mwat# dMlat dMout
* Printer 3
    UNTT 13 TYPE 25
```



## Observations :

- Linking is done by feeding upper hypocaust surfaces with outflowing energy rates (Pfree and Pfix) from the two zones and reciprocally feeding building with upper border temperatures (Tfree and Tfix) from hypocaust.
- Internal energy gains of hypocaust (PinH, PinH\#) and surrounding ground (PinG, PinG\#) are each defined by two alternative ways, so as to check for proper energy balance. Same is done for total free water within tubes (Mwat, Mwat\#) and energy diffused from zones to hypocaust (Pfree, Pfree\#, Pfix, Pfix\#).


## Results of simulation

Parameters defined further up and printed in output files are plotted hereafter and show following, expected dynamic :

- Airflow heats up hypocaust (see Fig. 3, $P s b l$ ). During first hours, energy diffuses from building and surrounding soil into colder hypocaust and as latter warms up diffusion reverses (see Fig. 4, Pfront, Pback, Pside, Pfree, Pfix).
- As airflow heats up hypocaust it cools down along the tubes (see Fig. 2, stratification of Tamb, T1-T4, Tout) and with time tends to reach equilibrium temperature.
- Warm and humid airflow condensates during first hours (see Fig. 3, Plat and Fig. 5, dMlat, Mlat). As ground temperature rises, all free water within tubes then evaporates again, after which no latent exchanges take place any more.
- Within Type 61 energy balance is correct (see Fig. 3, PinH, PinH\#, PinG, PinG\#), as is mass balance (see Fig. 5, Mwat, Mwat\#). Consistency of energy flows between modules is also respected (see Fig. 4, Pfree, Pfree\#, Pfix, Pfix\#).


Fig. 2: Temperature of air (Tfree, Tfix) and ground (TgFree, TgFix) of both zones as well as of airflow along the tubes (T1-T4) and at inlet and outlet (Tamb, Tout).


Fig. 3 : Internal heat gains of hypocaust (PinH, PinH\#) and surrounding soil (PinG, PinG\#), as well as energy entering hypocaust by airflow (Psbl, Plat) and diffused from ambient into surrounding soil (Pamb).


Fig. 4: Energy entering hypocaust from building (Pfree, Pfree\#, Pfix, Pfix\#) and from surrounding soil (Pfront, Pback, Pside).


Fig. 5 : Free water in tubes (Mwat, Mwat\#) as well as water condensation (dMlat) and flux out of tubes (dMout).

# TRNSYS compatible moist air hypocaust model 

## Part 3 : Source code

```
MaxSizes
PARAMETER(NIMax=40) ! max number of nodes along x [-]
PARAMETER(NJMax=100) !max number of nodes along y (per module) [-]
PARAMETER (NKMax=20) !max number of nodes along z (per module) [-]
PARAMETER (NtubMax=20) !max number of tubes (per module) [-]
PARAMETER(NsoilMax=10) !max number of soiltypes [-]
PARAMETER (NsurfMax=6) !max number of surfaces [-]
PARAMETER(NoptMax=100) !max number of optional outputs [-]
PARAMETER(NiniMax=20) !max number of initialisation conditions [-]
PhysConst
************************************************************************
REAL CmAir !specific heat of air [J/kg/K]
REAL CmWat !specific heat of water [J/kg/K]
REAL MmolAir !molar mass of air [kg/mol]
REAL MmolWat !molar mass of water [kg/mol]
REAL RhoWat !specific mass of water [kg/m3]
REAL Clatwat !latent heat of water [J/kg]
REAL CmVap ! specific heat of vapor [J/kg/K]
REAL Rgas !gas constant for water [J/mol/K]
COMMON/Type61PhysConst/
&CmAir, CmWat, MmolAix, MmolWat, RhoWat, ClatWat, CmVap, Rgas
!Files
```



```
INTEGER IparDef !unit number for parameter definition file [-1
INTEGER IparCon !unit number for parametex control file [-]
LOGICAL OparDef !initial status of parameter definition file [-]
LOGICAL OparCon !initial status of parameter control file [-]
COMMON/Type61Files/
&IparDef,IparCon,OparDef,oparCon
!Time
******
INTEGER Isim !general timestep number (Info(8)) [-]
INTEGER Irep !general timestep repetition number (Info(7)) [-]
REAL Dt !internal timestep [s]
REAL DtSoil !max internal timestep for soil [s]
REAL DtWat !max internal timestep for waterflow {s]
INTEGER IDt !internal timestep number [-]
INTEGER NDt inumber of internal timesteps [-]
COMMON/Type61Time/
&Isim,Irep,Dt,DtSoil,DtWat,IDt,NDt
!Geometry
**************************************************************************
INTEGER Nmod !number of modules [-]
INTEGER Nsec !number of cross-sections [-]
INTEGER TypSec(NIMax) !type of cross-sections along x [-]
INREGER NI ! number of nodes along x [-]
INTEGER NJ !number of nodes along y (per module) [-]
INTEGER NK !number of nodes along z (per module) [-]
REAL DX(0:NIMax+1) !node width along x {m]
REAL DY(0:NJMax+1) !node width along y {m]
REAL DZ(0:NKMax+1) !node width along z [m]
INTEGER I !node index along x [ - ]
IN2EGER J !node index along y [-]
INTEGER K !node index along z ["]
REAL LX !length [m]
REAL LY !lwiath [m)
REAL LZ !height [m]
INTEGER Idix !direction index (1-6) [-]
COMMON/Type61Geometry/
&Nmod,Nsec, TypSec,NI,NJ,NK, DX,DY,DZ,I,J,K, LX,LY,LZ,Idir
!Tubes
**************************************************************************
INTEGER Ntub !number of tubes (per module) [-]
INTEGER Itub !tube index {-]
INTEGER POSTub(NtubMax,2) !tube position (J,K index) [-]
REAL ThTub ! tube thickness [m]
REAL Ctub !tube circumfexence [m]
REAL CtubCor fcorrection factor for tube circumference [-]
REAL Dtub ! tube hydraulic diameter [m]
REAL VolTub !volume of tube node [m3]
REAL LamTub !tube conductivity [W/m/K]
REAL CVTub ! tube specific heat [J/m3/K]
REAL Ltub !tube length (m)
REAL DTtubTol !tolerance on tube node temperature [K]
REAL Sair !section of tube {m2}
REAL SairTot ltotal section of tubes (over all modules) [m2)
REAL Stub !surface of tube node [m2]
REAL StubTot !total surface of tubes (over all modules) [m2]
REAL Zair lairflow distribution factor (not normalised} [m5/2]
```

REAL ZairTot $:$ total of airflow distribution factors (over all modules) [m5/2] REAL Rfric !friction coefficent
COMMON/Type61Tubes/
\&Ntub, Itub, PosTub, ThTub, Ctub, CtubCor, Dtub, VolTub, LamTub, CvTub, Ltub, \&DTtubTol, Sair, SairTot, Stub, StubTot, Zair, ZairTot,Rfric
!Surfaces
INTEGER Nsurf ! number of surfaces [-]
REAL Xsurf (NsurfMax) !surface condition [degC or $W$ ]
REAL Xbord(NsurfMax) !border condition [W or degC]
REAL Kbord(Nsurfmax) !border conduction coefficient (W/K/m2)
REAL Sbord(Nsurfmax) !total border area [m2]
INTEGER TypSurf(NsurfMax) !type of surface condition [-]
REAL Rsurf(NsurfMax) !surface exchange coefficient [ $\mathrm{K} \mathrm{m} / \mathrm{W}$ ]
COMMON/Type61Surfaces/
\&Nsurf, Xsurf, Xbord, Kbord, Sbord, TypSurf, Rsurf
! Soil

INTEGER Nsoil ! number of soiltypes [-]
INTEGER Isoil !soil index [-]
REAL TSoilo (NIMax, NJMax, NKMax)
!initial soil temperature for TRNSYS timestep [degC]
REAL Tsoill(0:NIMax+1,0:NJMax+1,0:NKMax+1)
!initial soil temperature for internal timestep [degc]
REAL Tsoil2 (NJMax, NJMax, NKMax)
!final soil temperature for internal timestep [degc]
INTEGER TypSoil(0:NIMax+1, 0:NJMax+1, 0:NKMax+1) !type of soil/surf. [-]
REAL VolSoil inode volume (m3]
REAL Ssoil(6) !lateral area of node [m2]
REAL Ksoil(6) : conduction coefficient to neighbour node [ $\mathrm{W} / \mathrm{m} 2 / \mathrm{K}$ ]
REAL LamSoil(Nsoilmax) !soil conductivity [ $\mathrm{W} / \mathrm{m} / \mathrm{K}$ ]
REAL CvSoil (NsoilMax) isoil specific heat [J/m3/K]
COMMON/TYpe61Soil/
\&Nsoil, Isoil, Tsoilo,Tsoill,Tsoil2,TypSoil, VolSoil, Ssoil, Ksoil,
\&LamSoil, CvSoil
: Air
INTEGER Iflow tairflow index (-)
INTEGER IflowIni ! I index of tube beginning $[-]$
INTEGER IflowEnd ! I index of tube end [-]
INTEGER DirAir !direction of airflow [-]
REAL Fair ! tube airflow (m3/s)
REAL Fairtot ! total airflow (over all modules) [m3/s]
REAL Fairmin !min airflow (over all modules) [m3/s]
REAL FairminTub !min airflow for stability [m3/s]
REAL Vair !air velocity (m/s)
REAL Kair laix/tube exchange coefficient [W/m2/K]
REAL Kair0 !air/tube constant exchange coefficient [ $\mathrm{W} / \mathrm{m} 2 / \mathrm{K}$ ]
REAL Kairl !air/tube linear exchange coefficient [ $(\mathrm{W} / \mathrm{m} 2 / \mathrm{K}) /(\mathrm{m} / \mathrm{s})]$
REAL RhoAir ! specific weight of air [ $\mathrm{kg} / \mathrm{m} 3$ ]
REAL PrAir !air pressure [Pa]
REAL DPrAir t total air pressure loss [Pa]
REAL Tair !air temperature \{degC]
REAL TairIn tair temperature at hypocaust inlet [degC]
REAL TairOut !aix temperature at hypocaust outlet [degC]
REAL Hrel ! relative humidity (pcent.]
REAL Hrelin !relative humidity at inlet [pcent]
REAL HrelOut !relative humidity at outlet [pcent]
REAL Habs !absolute humidity [Pal
REAL HabsIn !absolute humidity at inlet [Pa]
REAL HabsOut !absolute humidity at outlet [Pa]
REAL Hrat ! humidity ratio [kg vapor/kg air]
REAL Hrat In ! humidity ratio at inlet $\{\mathrm{kg}$ vapor $/ \mathrm{kg}$ air]
REAL Hratout ! humidity ratio at outlet [ kg vapor/ kg air]
REAL Hsat !saturating pressure [Pa]
REAL Hsatin !saturating pressure at inlet [Pa]
REAL Hsatout !saturating pressure at outlet [Pa]
COMMON/Type61Air/
\&Iflow, IflowIni, Iflowend, DirAir, Fair, FairTot, FairMin, FairMinTub,
\&Vair, Kair, Kairo, Kair1, RhoAir, PrAir, DPrAir, Tair, TairIn, Tairout, \&Hrel, Hrelin, HrelOut, Habs, HabsIn, HabsOut, Hrat, HratIn, HratOut,
\&Hsat, Hsatin, Hsatout.
! Water
REAL Vwat (-1:1) !velocity of waterflow (for each airflow type) [m/s] INTEGER TypWat (-1:1) !type of waterflow (for each airflow type) [-]
REAL Fwatinftot ! total water infiltration (over all modules) [m3/s)
REAL Sinftot !total surface of water infiltration (over all modules) (m2)
INTEGER POSInf(6) !position of watex infiltration [-]
REAL Mwato (NIMax, NtubMax)

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!initial watermass for TRNSYS timestep [kg]
REAL Mwat 1 (NIMax, NtubMax)
!initial watermass for internal timestep $[\mathrm{kg}]$
REAL Mwat2 (NIMax, NtubMax)
!final watermass for internal timestep [kg]
REAL MwatLat !mass of water cond. levap. in node [kg]
REAL MwatIn !mass of water flowing into node [kg]
REAL MwatInf !mass of water infiltrating into node $[\mathrm{kg}]$
REAL MwatOut !mass of water flowing out of node [kg]
COMMON/Type61Water/
\&Vwat, Typhat, FwatinfTot, SinfTot, PosInf, Mwat0, Mwat1, Mwat2،
\&MwatLat, MwatIn, Mwatinf, MwatOut.

```
! Energy
REAL PSbl !sensible power from airflow [W]
REAL Plat !latent power from airflow [W)
REAL Psoil(0:6) !diffusive power from neighbor nodes/surfaces [W]
REAL Pwat !diffusive power from free water [W]
REAL Pfric !power from frictional losses [W]
REAL Pint !internal power [W]
REAL PsblTot !total sensible power (over all modules) [W]
REAL PlatTot !total latent power (over all modules) (W)
REAL PsurfTot !total diffusive power from surfaces (over all modules) [W]
REAL PwatTot !total diffusive power from free water (over all modules) [W)
REAL PfricTot :total power from frictional losses (over all modules) [W]
REAL PintTot :total internal power (over all modules) [W]
COMMON/Type61Energy/
&Psbl,Plat,Psoil, Pwat,Pfric,Pint,PsblTot,PlatTot,PsurfTot,PwatTot,
&PfricTot,PintTot
!Initialisation
!***********************************************************************
INTEGER NiniSoil !number of initial temperatures [-]
INTEGER NiniWat ! number of initial water thicknesses [-]
REAL TiniSoil(NiniMax) !initial temperatures [degC]
REAL ThIniWat(NiniMax) initial water thicknesses [m]
INTEGER POSIniSoil(Ninimax,6) !position of initial temperatures [-]
INTEGER POSIniWat(Ninimax,6) !position of initial water thicknesses [-)
INTEGER Iini !initialisation index {-]
COMMON/TYpe61Initialisation/
&NiniSoil,NiniWat,TiniSoil,ThIniWat,PosIniSoil, PosIniWat,Iini
!Optionals
*************************************************************************
INTEGER Nopt {number of optional outputs [-]
INTEGER TypOpt(NoptMax) !type of optional output [-]
INTEGER POSOpt(NoptMax,6) !position of optional output [-]
REAL Opt(NoptMax) !optional output (fct of Typopt]
INTEGER Iopt !optionals index [-]
COMMON/Type610ptionals/
&Nopt, TypOpt, PosOpt,Opt,Iopt
```


SUBROUTINE TYpe61 (Time, Xin, Xout, T, DtDt, Par, Info, Icntrl,*)
IVERSION : 1.0
!DESCRIPTION
! Hypocaust model describing sensible and latent exchange between
la moist airflow and a buried pipe system, with possibility to
!use both air directions.
!
IAUTHOR :
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!ch - 1205 Geneve
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!common variables:
!--------------------
INCLUDE 'type61.inc'
!local variables:
1--------...............--
DOUBLE PRECISION Xin(5+NsurfMax)
DOUBLE PRECISION Xout(4+NsurfMax+NoptMax)
REAL Time, T, DtDt
REAL Par ( $5+2$ *NsurfMax)
INTEGER*4 Info(15)
INTEGER Icntri

!checking/conversion of arguments:

CALL CheckConnections (Info)
CALL ConvertInput (Time, Xin, Par, Info)
!initialisation / normal timestep:
!----------------------------------
IF (Isim.EQ.1) THEN !initialisation
!set constants:
CALL SetPhysicalConstants
!set parameters:
CALL OpenParameterFiles
CALL ReadSuppliedParameters
CALL SetDerivedParameters
CALL SetSimulationParameters
CALL CloseParameterfiles
!initialise soil \& water:
CALL InitialiseSoil
CALL Initialisewater
ELSE !normal timestep
CALL ResetOutputs
DO IDE $=1$, NDE
!updates from previous timestep/surfaces:
CALL UpdateSoil
CALL UpdateWater
CALL SetSurfaces
!evolution of air/tube
DO Itub=1, Ntub
CALL AirInput
DO Iflow=IflowIni, Iflowend
CALI TubeProperties
CALL TubeEvolution
CALL OptionalsTube
END DO
CALE AirOutput
END DO
!evolution of soil:
DO $I=1$, NI
DO $J=1$, NJ
DO K=1,NK
IF (TYpSOil(I,J,K).NE.0) THEN
CALL SoilProperties
CALL Soilevolution
CALL OptionalsSoil
CALL SetBorders
END IF
END DO

END DO END DO
!miscellaneous:
CALL OptionalsMiscellaneous
END DO

END IF
!checking/conversion of arguments:
CALL ConvertOutput (Xout)
RETURN
END


SUBROUTINE CheckConnections (Info)
!common variables:
!....----------------
!local variables:

INTEGER*4 Info(15)
CHARACTER*3 Ycheck(5+NsurfMax), Ocheck (4+NsurfMax+NoptMax)

lUnits for optional outputs are read in parameter file during
!lst simulation step, so checking can only be done at 2nd step:
IF (Isim.EQ.2) THEN
! Ycheck:
Ycheck $(1)={ }^{+} \mathrm{VF} 1$ ' : FairTot $[\mathrm{m} 3 / \mathrm{hr}]$
Ycheck $\{2\}={ }^{\text {'T TE1' }}$ !TairIn [degC]
Ycheck $\{3\}=$ 'PC1' !HrelIn [pcent]
Ycheck(4)='PR1' !PrAix [bar]
Ycheck $(5)=$ 'VF1, ! FwatInfTot (m3/hr) DO Isurf=1, Nsur£Max

IF (TypSurf(Isurf).EQ.0) THEN
Ycheck $(5+$ Isurf $)=$ 'TE1' !Xsurf [degC]
ELSE
Ycheck(5+Isurf) $=$ 'RW1' !Xsurf [kJ/hr]
END IF
END DO
! ocheck:
!
Ocheck(1)='TE1' !TairOut [degC]
Ocheck(2)='PCl' !Hxelout [pcent]
Ocheck $\{3$ ) $=$ 'PW1' : PsblTot $\{\mathrm{kJ} / \mathrm{hr}\}$
Ocheck $(4)=$ 'PW1' !platTot $[\mathrm{kJ} / \mathrm{hr}]$
DO Xsurf=1,NsurfMax
IF (TypSurf(Isurf).EQ.0) THEN
Ocheck $(5+I \operatorname{suxE})=$ 'PW1' : Xbord [kJ/hr]
ELSE
Ocheck(5+Isurf)='TE1' !Xbord [degC]
END IF
END DO
DO Iopt=1, NoptMax
! Tube:
IF (Typopt (Iopt).EQ. 1) Ocheck (Iopt)='TE1' ITaix [degC]
IF (TypOpt (Iopt).EQ. 2) Ocheck(Iopt)='PCl' !Hzel [pcent]
IF (TypOpt (Iopt).EQ. 3) Ocheck(Iopt)='PR1'
IF (Typopt (Iopt).EQ. 4) Ocheck (Iopt) $=$ 'DM1'
IF (Typopt (Iopt).EQ. 5) Ocheck(Iopt) ='VLl'
IF (TypOpt (Iopt). EQ. 6) Ocheck (Iopt)='VF1'
IF (Typopt (Iopt).EQ. 7) Ocheck(Iopt) ='VF1'
IF (Typopt (Iopt).EQ. 8) Ocheck (Iopt)='VF1'
IF (Typopt (Iopt).EQ. 9) Ocheck(Iopt)='VF1'
IF (TypOpt(Iopt).EQ. 10) Ocheck(Iopt)='TE1'
IF (Typopt (Iopt).EQ. 11) ocheck(Iopt) ='PW1.
IF (Typopt (Iopt).EQ. 12) Ocheck (Iopt) $=$ 'PW1.
IF (TypOpt (Iopt).EQ. 13) Ocheck(Iopt)='PW1'
IF (Typopt (Iopt).EQ. 14) Ocheck(Iopt) ='PW1'
IF (TypOpt(Iopt).EQ. 15) Ocheck (Iopt)='PW1,
IF (TypOpt (Iopt).EQ. 16) Ocheck(Iopt) ='PW1' IF (Typopt (Iopt).EQ. 17) Ocheck(Iopt)='PW1'
IF (Typopt \{Iopt).EQ. 18) Ocheck (Iopt $\rangle=$ 'PW1'
IF (TypOpt(Iopt).EQ. 19) Ocheck(Iopt)='PW1'
IF (Typopt(Iopt).EQ. 20) Ocheck(Iopt)='PW1'
IF (Typopt(Iopt).EQ. 21) Ocheck(Iopt)='PW1.
IF (Typopt (Iopt).EQ. 22) Ocheck(Iopt)='PW1'
IF (TypOpt(Iopt).EQ. 23) Ocheck(Iopt)='VFI'
!Habs [bar]
! Hrat [kg vapor/kg air]
! Mwat [m3]
!MwatLat [m3/hr]
! Mwat In [m3/hx]
! MwatInf $[\mathrm{m} 3 / \mathrm{hr}$ ]
!MwatOut [m3/hr]
!Tsoil [degC]
! Psbl [kJ/hr]
!Plat [kJ/hr]
! Pwat [kJ/hr]
!Pfric [kJ/hr]
!Psoil(0) [kJ/hr]
!Psoil(1) [kJ/hr]
!Psoil (2) $[\mathrm{kJ} / \mathrm{hr}]$
! Psoil (3) [kJ/hr]
!Psoil(4) [kJ/hr]
!Psoil(5) [kJ/hr]
!Psoil (6) [kJ/hr]
!Pint [kJ/hr]
Pair [m3/hr]
C previous line is replaced by following ones because of a bug
in main TRNSYS program, version 14.1 and 14.2 , which resets Info(7)
to 0 at the end of lst timestep.
IF (Isim.EQ.1) THEN
Irep $=-1$
TimePrev=Time
ELSE IF (Time.EQ.TimePrev) THEN
Irep=Irep+1
ELSE
Irep=0
TimePrev=Time
END IF
Info(6) $=5+$ Nsurfmax + NoptMax
! Parameters:
----~-.....--
IF (Isim.EQ.1) THEN
IparDef=INT $\{\operatorname{Par}(1))$ ! [-]
Iparcon=INT $(\operatorname{Par}(2))$ ! [-]
Dt=Par (3)*3600 ! [s] <- [hr]
FairMin $=\operatorname{Par}(4) / 3600$ ! $[\mathrm{m} 3 / \mathrm{s}]<-\{\mathrm{m} 3 / \mathrm{hr}\}$
DTtubTol=Par (5) ! (K)
DO Isurf $=1$, Nsurfmax
TypSurf(Isurf) $=\operatorname{Par}(5+$ Isurf $)$ ! [-]
END DO
DO Isurf=1, Nsurfmax
Rsurf(Isurf) $=\operatorname{Par}(5+$ NsurfMax+Isurf) $/ 3.6$ : $[\mathrm{W} / \mathrm{m} 2 \mathrm{~K}]<-[\mathrm{kJ} / \mathrm{hr} \mathrm{m} 2 \mathrm{~K}]$
END DO
END IF
! Inputs:
1--2---
FairTot=0
DirAir=0
IF (Info(8).GT. 1) THEN
IF (ABS (Xin(1)/3600). GE.FairMin) THEN
FairTot=ABS (Xin(1)/3600) ! [m3/s] <- [m3/hr]
DirAir=INT(Xin(1)/ABS (Xin(1) )) ! [-]
END IF
END IF
TairIn=Xin(2) ! [degC]

```
    Hre1In=Xin(3) ! [pcent]
```

    Hre1In=Xin(3) ! [pcent]
    PrAir=Xin(4)*1E5 ! [Pa] <- [bar]
    PrAir=Xin(4)*1E5 ! [Pa] <- [bar]
    IF (Info(8).GT.1) THEN
    IF (Info(8).GT.1) THEN
        FwatInfTot=Xin(5)/3600 : [m3/s] <- [m3/hr]
        FwatInfTot=Xin(5)/3600 : [m3/s] <- [m3/hr]
    ELSE
    ELSE
        FwatInfTot=0
        FwatInfTot=0
    END IF
    END IF
    DO Isurf=1,NsurfMax
    DO Isurf=1,NsurfMax
        IF (TypSurf(Isurf).EQ.0) THEN
        IF (TypSurf(Isurf).EQ.0) THEN
        Xsurf(Isurf)=Xin(5+Isurf) ! [degC] <- [degC]
        Xsurf(Isurf)=Xin(5+Isurf) ! [degC] <- [degC]
        ELSE
        ELSE
        Xsurf(Isuxf) =Xin(5+Isurf)/3.6 ! [W]<- [kJ/hr]
        Xsurf(Isuxf) =Xin(5+Isurf)/3.6 ! [W]<- [kJ/hr]
        END TF
        END TF
    END DO
    END DO
    RETURN
    RETURN
    END
    END
    C******************************************************************************
C******************************************************************************
C*******************************************************************************
C*******************************************************************************
SUBROUTINE ConvertOutput(Xout)
SUBROUTINE ConvertOutput(Xout)
!common variables:
!common variables:
!------n-------------
!------n-------------
INCLUDE 'type61.inc'
INCLUDE 'type61.inc'
!local variables:
!local variables:
!--.------------------
!--.------------------
DOUBLE PRECISION Xout (4+NsurfMax+NoptMax)

```
    DOUBLE PRECISION Xout (4+NsurfMax+NoptMax)
```




```
    Xout (1)=Tairout ! [degC]
```

    Xout (1)=Tairout ! [degC]
    Xout(2)=HrelOut ! [pcent]
    Xout(2)=HrelOut ! [pcent]
    Xout(3)=PsblTot*3.6 ! [kJ/hr] <- [W]
    Xout(3)=PsblTot*3.6 ! [kJ/hr] <- [W]
    Xout(4)=PlatTot*3.6 ! [kJ/hr] <- [W]
    Xout(4)=PlatTot*3.6 ! [kJ/hr] <- [W]
    DO Isurf=1,Nsurf
    DO Isurf=1,Nsurf
        IF (TypSurf(Isurf).EQ.0) THEN
        IF (TypSurf(Isurf).EQ.0) THEN
        Xout(4+Isurf) =Xbord(Isurf)*3.6 ! [kJ/hr] <- [W]
        Xout(4+Isurf) =Xbord(Isurf)*3.6 ! [kJ/hr] <- [W]
        ELSE
        ELSE
        Xout(4+Isurf) =Xbord(Isurf) ! [degC)
        Xout(4+Isurf) =Xbord(Isurf) ! [degC)
        END IF
        END IF
    END DO
    END DO
    DO Iopt=1,Nopt
    DO Iopt=1,Nopt
        Xout(4+NsurfMax+Iopt)=Opt(Iopt) ! cf. SetOptional for units
        Xout(4+NsurfMax+Iopt)=Opt(Iopt) ! cf. SetOptional for units
    END DO
    END DO
    RETURN
    RETURN
    END
    END
    C*********************************************************************************
C*********************************************************************************
SUBROUTINE ResetOutputs
SUBROUTINE ResetOutputs
!common variables:
!common variables:
!-----------------m
!-----------------m
INCLUDE 'type61.inc'

```
    INCLUDE 'type61.inc'
```




```
    PsblTot=0
```

    PsblTot=0
    PlatTot=0
    PlatTot=0
    PsurfTot=0
    PsurfTot=0
    PwatTot=0
    PwatTot=0
    PfricTot=0
    PfricTot=0
    PintTot=0
    PintTot=0
    DO Isurf=1,Nsurf
    DO Isurf=1,Nsurf
        Xbord(Isurf) =0
        Xbord(Isurf) =0
    END DO
    END DO
    DO Iopt=1,Nopt
    DO Iopt=1,Nopt
        Opt (Iopt)=0
        Opt (Iopt)=0
    END DO
    END DO
    RETURN
    RETURN
    END
    END
    C******************************************************************************
C******************************************************************************
C*****************************************************************************
C*****************************************************************************
SUBROUTINE UpdateSoil
SUBROUTINE UpdateSoil
!common variables:
!common variables:
!--------------------
!--------------------
INCLUDE 'type61.inc'

```
    INCLUDE 'type61.inc'
```




```
    IF (IDE.EQ.1) THEN
```

```
    IF (IDE.EQ.1) THEN
```

```
    !reset:
    DO I=1,NI
    DO J=1,NJ
    DO K=1,NK
        IF (Irep.EQ.0) THEN
                Tsoil0(I,J,K)=Tsoil2(I,J,K)
            END IF
            Tsoill(I,J,K)=TsoilO(I,J,K)
        END DO
        END DO
        END DO
    ELSE
        !update:
        DO I=1,NI
        DO J=1,NJ
        DO K=1,NK
            Tsoil1(I,J,K)=Tsoil2(I,J,K)
        END DO
        END DO
        END DO
    END IF
    RETURN
    END
C********************************************************************************
C******************************************************************************
    SUBROUTINE UpdateWater
    !common variables:
    --------------.".-.
```



```
    IF (IDt.EQ.1) THEN
        !reset:
        DO I=IflowIni,IflowEnd
            DO Itub=1,Ntub
            IF (Irep.EQ.0) THEN
                Mwat0(I,Itub)=Mwat2 (I, Itub)
                END IF
            Mwat1 (I, Itub)=Mwat0(I,Itub)
        END DO
        END DO
    ELSE
        !update:
        DO I=IflowIni,IflowEnd
        DO Itub=1,Ntub
            Mwat:1 (I, Itub)=Mwat2 (I, Itub)
        END DO
        END DO
    END IF
    RETURN
    END
C*****************************************************************************
    SUBROUTTNE SetSurfaces
    !common variables:
    !-\cdots.---------------
    !local variables:
    !-----------*---------
    INTEGER Isurf
```



```
    DO I=1,NI
    DO J=1,NJ
        Isurf=TypSoil(I,J,0)
        IF (Isurf.GT.0) THEN
        IF (TypSurf(Isurf).EQ.0) THEN !input temperature:
                Tsoill(I,J,0)=Xsurf(Isurf)
            ELSE !input power:
                Tsoill(I,J,0) =Tsoill(I,J,1)
                +Xsurf(Isurf)/Sbord(Isurf)/Kbord(Isurf)
            END IF
        END IF
        Isurf=TypSoil(I,J,NK+1)
        IF (Isurf.GT.0) THEN
            IF (TypSurf(Isurf).EQ.0) THEN !input temperature:
                Tsoill(I,J,NK+1)=Xsurf(Isurf)
            ELSE !input power:
                Tsoil1(I,J,NK+1)=Tsoil1(I,J,NK)
```

```
    &
                +Xsurf(Isurf)/Sbord(Isurf)/Kbord(Isurf)
            END IF
        END IF
    END DO
    END DO
    DO I=1,NI
    DO K=1,NK
        Isurf=TypSoil(I,O,K)
        IF (Isurf.GT.0) THEN
        IF (TypSurf(Isurf).EQ.0) THEN !input temperature:
            Tsoill(I,0,K) =Xsurf(Isurf)
            ELSE !input power:
                    Tsoil1(I,0,K)=Tsoil1(I, 1,K)
                    +Xsurf(Isurf)/Sbord(Isurf)/Kbord(Isurf)
            END IF
        END IF
    Isurf=TypSoil (I,NO+1,K)
    IF (Isurf.GT.0) THEN
        IF (TypSurf(Isurf).EQ.O) THEN !input temperature:
                Tsoill(I,NJ+1,K)=Xsurf(Isurf)
            ELSE !input power:
                TSOil1(I,NJ+1,K)=TSOill1(I,NJ,K)
    &
                +Xsurf(Isurf)/Sbord(Isurf)/Kbord(Isurf)
            END IF
        END IF
    END DO
    END DO
    DO J=1,NJ
    DO K=1,NK
    Isurf=TypSoil(0,J,K)
    IF (Isurf.GT.0) THEN
            IF (TypSurf(Isurf).EQ.O) THEN !input temperature:
            Tsoil1(0,J,K)=Xsurf(Isurf)
            ELSE !input power
                    Tsoill(0,J,K)=Tsoill(1,J,K)
                    +Xsurf(Isurf)/Sbord(Isurf)/Kbord(Isurf)
            END IF
        END IF
        Isurf=TypSoil(NI+1,`,K)
    IF (Isurf.gT.0) THEN
            IF (TYpSuxf(Isuxf).EQ.O) THEN !input temperature:
            Tsoil1(NI+1,J,K)=Xsurf(Isurf)
            ELSE !input power:
                    Tsoil1(NI+1,J,K)=Tsoil1(NI,J,K)
                    +Xsurf(Isurf)/Sbord(Isurf)/Kbord(Isurf)
            END IF
        END IF
    END DO
    END DO
    RETURN
    END
C********************************************************************************
C*******************************************************************************
    SUBROUTINE AirInput
    !common variables:
    !~---m---~----------
    INCLUDE 'type61.inc'
    !local variables:
    !---n----~------------
    REAL Hsat$,Hrat$,Habs$
```



```
    IF ({IDL.EQ.1).AND.(ItUb.EQ.1)) THEN
        !psychometrics:
        HsatIn=Hsat$(TairIn)
        HabsIn=HrelIn*HsatIn/100
        HratIn=Hrat$ (HabsIn, PrAir)
        !general flow variables:
        RhoAir=PrAir*MmolAir/Rgas/(Tair+273.15)
        DPrAir=Rfric*Ltub*RhoAir/2*(FairTot/ZairTot)**2
        PEricTot=FairTot*DPrAix
        END IF
```

529 531 531

```
    Tair=Taixin
```

    Tair=Taixin
    Hrel=HrelIn
    Hrel=HrelIn
    Hsat=HsatIn
    Hsat=HsatIn
    Habs=HabsIn
    Habs=HabsIn
    Hrat=HratIn
    Hrat=HratIn
    Iflow=IflowIni
    Iflow=IflowIni
    CALL TubeProperties
    CALL TubeProperties
    Faix=FairTot*Zair/ZairTot
    Faix=FairTot*Zair/ZairTot
    Vair=Fair/Sair
    Vair=Fair/Sair
    Kair=Kair0+Kair1*Vair
    Kair=Kair0+Kair1*Vair
    RETURN
    RETURN
    C**********************************************************************************
C**********************************************************************************
***********************************************************************
***********************************************************************
SUBROUTINE TubeProperties
SUBROUTINE TubeProperties
!common vaxiables:
!common vaxiables:
!--------------------
!--------------------
INCLUDE 'type61.inc'

```
    INCLUDE 'type61.inc'
```




```
    IF (DirAir.GE.0) THEN
```

    IF (DirAir.GE.0) THEN
        I=Iflow
        I=Iflow
    ELSE
    ELSE
        I=IflowEnd+IflowIni-Iflow
        I=IflowEnd+IflowIni-Iflow
    END IF
    END IF
    J=PosTub(Itub,1)
    J=PosTub(Itub,1)
    K=PosTub(Itub,2)
    K=PosTub(Itub,2)
    IF ((J.EQ.1).OR.(J.EQ.NJ)) THEN
    IF ((J.EQ.1).OR.(J.EQ.NJ)) THEN
        Ssoil(1)=(2*DY(J) +DZ(K))*CtubCor*ThTub
        Ssoil(1)=(2*DY(J) +DZ(K))*CtubCor*ThTub
        Ssoil(2)=(2*DY(J)+DZ(K))*CtubCor*ThTub
        Ssoil(2)=(2*DY(J)+DZ(K))*CtubCor*ThTub
    ELSE
    ELSE
        Ssoil(1)=2*(DY(J)+DZ(K))*CtubCor*ThTub
        Ssoil(1)=2*(DY(J)+DZ(K))*CtubCor*ThTub
        Ssoil(2)=2*(DY(J) +DZ(K))*CtubCor*ThTub
        Ssoil(2)=2*(DY(J) +DZ(K))*CtubCor*ThTub
    END IF
    END IF
    IF (I.EQ.IflowIni) THEN
    IF (I.EQ.IflowIni) THEN
        Ksoil(1)=0
        Ksoil(1)=0
    ELSE
    ELSE
        Ksoil(1)=2*LamTub/(DX(I-1)+DX(I))
        Ksoil(1)=2*LamTub/(DX(I-1)+DX(I))
    END IF
    END IF
    IF (I.EQ.IflowEnd) THEN
    IF (I.EQ.IflowEnd) THEN
        Ksoil(2)=0
        Ksoil(2)=0
    ELSE
    ELSE
        Ksoil(2)=2*LamTub/(DX(I+1) +DX(I))
        Ksoil(2)=2*LamTub/(DX(I+1) +DX(I))
    END IF
    END IF
    IF (J.EQ.1) THEN
    IF (J.EQ.1) THEN
        Ssoil(3)=0
        Ssoil(3)=0
        Ksoil(3)=0
        Ksoil(3)=0
    ELSE
    ELSE
        Ssoil(3)=DX(I)*DZ(K)*CtubCor
        Ssoil(3)=DX(I)*DZ(K)*CtubCor
        Ksoil(3)=1/(DY(J-1)/2/LamSoil(TypSoil(I,J-1,K)) +ThTub/LamTub)
        Ksoil(3)=1/(DY(J-1)/2/LamSoil(TypSoil(I,J-1,K)) +ThTub/LamTub)
    END IF
    END IF
    IF (J.EQ.NJ) THEN
    IF (J.EQ.NJ) THEN
        Ssoil(4)=0
        Ssoil(4)=0
        Ksoil(4)=0
        Ksoil(4)=0
    ELSE
    ELSE
        Ssoil(4)=DX(I)*DZ(K)*CtubCor
        Ssoil(4)=DX(I)*DZ(K)*CtubCor
        Ksoil(4)=1/(DY(J+1)/2/LamSoil(TypSoil(I,J+1,K))+ThTub/LamTub)
        Ksoil(4)=1/(DY(J+1)/2/LamSoil(TypSoil(I,J+1,K))+ThTub/LamTub)
    END IF
    END IF
    Ssoil(5)=DX(I)*DY (J)*CtubCor
    Ssoil(5)=DX(I)*DY (J)*CtubCor
    Ksoil(S)=1/(DZ(K-1)/2/LamSoil(TypSoil(I,J,K-1))+ThTub/LamTub)
    Ksoil(S)=1/(DZ(K-1)/2/LamSoil(TypSoil(I,J,K-1))+ThTub/LamTub)
    Ssoil(6)=DX(I)*DY(J)*CtubCor
    Ssoil(6)=DX(I)*DY(J)*CtubCor
    Ksoil(6)=1/(DZ(K+1)/2/LamSoil(TypSoil (I,J,K+1))+ThTub/LamTub)
    Ksoil(6)=1/(DZ(K+1)/2/LamSoil(TypSoil (I,J,K+1))+ThTub/LamTub)
    Sair=DY(J)*DZ(K)
    Sair=DY(J)*DZ(K)
    VolTub=Ssoil(1)*DX(I)
    VolTub=Ssoil(1)*DX(I)
    Stub=Ssoil(3)+Ssoil(4) +Ssoil(5)+Ssoil(6)
    Stub=Ssoil(3)+Ssoil(4) +Ssoil(5)+Ssoil(6)
    Ctub=Stub/DX(I)
    Ctub=Stub/DX(I)
    Dtub=4*Sair/Ctub
    Dtub=4*Sair/Ctub
    Zair=Sair*SQRT(Dtub)
    Zair=Sair*SQRT(Dtub)
    RETURN
    RETURN
    C********************************************************************************
C********************************************************************************
C*****************************************************************************
C*****************************************************************************
SUBROUTINE TubeEvolution
SUBROUTINE TubeEvolution
!common variables:
!common variables:
------------------
------------------
INCLUDE 'type61,inc'

```
    INCLUDE 'type61,inc'
```

```
!local variables:
```



```
ReAL Hsat\$, Hrat\$, Habs\$
REAL MwatSat ! mass of water necessary to satuarte node aix [kg] REAL MwatLew ! theoretical mass of water cond./evap. in node [kg]
```



```
!input water:
!------------
!flow from previous node:
IF (Iflow.EQ.IElowini) THEN Mwat \(\mathrm{In}=0\)
ELSE IF (TypWat(DirAir).EQ.1) THEN ! flow Mwat In=Mwatout
ELSE !ejection MwatIn=0
END IF
!infiltxation
Mwatinf=0
IF ((I.GE. PosInf(1)).AND. (I.LEE.POSInf(4))) THEN
IF ((J.GE.Posinf (2)).AND. (J.LE.PosInf(5))) THEN
IF ((K.GE.PosInf(3)).AND. (K.LE.PosInf(6))) THEN
MwatInf=FwatInfTot*Dt*Rhowat*Stub/SinfTot
END IF
END \(I F\)
END IF
!energy balance of tube :
DTaixtub \(=\operatorname{MAX}(\operatorname{ABS}(T a i x-T s o i l 1(I, J, K)), 0.5)\)
Tmax=Tair+DTairtub
Tmin=Tair-DTairtub
Ibal=0
DO WHILE (Ibal.NE.2)
CALL FindZero(Balance, Tsoil2(I, J, K), Tmin, Tmax, DTtubTol, Ibal)
IF (Ibal.EQ.3) THEN
DTairtub=2*DTairtub GOTO 100
END IF
llatent and sensible heat from air:
IF (DirAix.NE. 0 ) THEN
HratSatTub=Hrat\$ (Hsat\$(Tsoil2 (I, J, K)), PrAir)
HratSatAir=Hrat\$(Hsat\$(Tair), PrAir)
IF ((Hrat.GT.HratSatTub).OR. (Hxat.GT.HratSatAir)) THEN
! condensation:
MwatLew=Dt*(Hrat-HratSatTub) *Kair*Stub/CmAir
MwatSat=(Hrat-HratSatAir) *RhoAir*Sair*Vair*Dt
MwatLat=MAX (MwatLew, MwatSat) ELSE
!evaporation:
MwatLew=Dt*(HratSatTub-Hrat) *Kaix*Stub/CmAir
MwatSat \(=(\) HratSatAix-Hrat)*RhoAir*Sair*Vair*Dt
MwatLat \(=-\) MIN (MwatLew, MwatSat, Mwat1 (I, Itub) +MwatIn+MwatInf)
END IF
Plat=ClatWat*MwatLat/Dt
Psbl=Stub*Kair*(Tair-Tsoil2 (I, J, K) )
ELSE
MwatLew=0
MwatSat=0
MwatLat=0
Plat=0
Psbl \(=0\)
END IF
!diffusive heat from water:
Pwat = (Mwat1 (I, Itub)*(Tsoill(I,J,K) -Tsoil2(I,J,K))
+MwatIn *(Tsoil2(I-DirAir, J,K)-Tsoil2 (I, J, K) ))
*CmWat/Dt
!diffusive heat from soil:
Psoil (1) =Ksoil(1)*Ssoil(1)*(Tsoil1(I-1,J,K) -Tsoil2 (I,J,K))
Psoil \((2)=\) Ksoil \((2) * \operatorname{Ssoil}(2) *(\) Tsoill \((I+1, J, K)-T s o i l 2(I, J, K))\)
```



```
Psoil (4) =Ksoil (4)*Ssoil(4)* (Tsoill (I, J+1, K)-Tsoil2 (I, J, K))
Psoil (5) \(=\operatorname{Ksoil}(5) * \operatorname{Ssoil}(5) *(T \operatorname{soill}(I, J, K-1)-T \operatorname{soil2}(I, J, K))\)
Psoil (6) \(=\) Ksoil \((6) * \operatorname{Ssoil}(6) *(\) Tsoill \((I, J, K+1)-T s o i l 2(I, J, K))\)
Psoil (0) =Psoil(1) +Psoil (2) +Psoil(3)+Psoil(4) +Psoil (5) + Psoil (6)
internal heat:
Pint=CvTub*VolTub* (Tsoil2 (I, J, K)~Tsoill(I,J,K))/Dt
```

!energy balance:
Balance=Pint-Plat-Psbl-Psoi1(0)-Pwat

END DO
!update Tsoill (equivalence of Psoil in routines TubeEvolution and Soilevolution $:$ $\operatorname{Tsoil1}(I, J, K)=T \operatorname{soi} 12(I, J, K)$
!mass balance of water:

IF (TypWat(DirAir).EQ.1) THEN !flow
MwatOut = (Mwatl (I, Itub) +MwatLat+MwatIn+MwatInf)
$\&$
Vwat (DirAir) *Dt/DX(I)
ELSE !ejection
MwatOut=Mwat1 (I, Itub) +MwatLat+MwatIn+MwatInf
END TE
Mwat2 (I, Itub $)=$ Mwat 1 (I, Itub $\rangle$ +MwatLat+MwatIn+MwatInE-Mwatout-Mwateje
!energy balance of air :
----
IF (DirAir.NE.0) THEN
P£ric=pexicTot* (Fair/FairTot) * (DX (I)/Etub)
Tair=Tair+(Pfric-Psbl)/(CmAir+Hrat*CmVap)/(RhoAir*Sair*Vair)
Hrat=Hrat-MwatLat/(RhoAir*Saix*Vaix*Dt)
Habs=Habs\$(Hrat, PrAir)
Hsat=Hsat\$ (Tair)
$\mathrm{Hrel}=100^{*} \mathrm{Habs} / \mathrm{Hsat}$
ELSE
Pfric=0
Taix=TairIn
Hrat=HratIn
Habs=HabsIn
Hsat=HsatIn
Hrel=HrelIn
END IF
!integrals :
----------
PsblTot $=$ PsblTot+Psbl*Nmod/NDt PlatTot $=$ PlatTot+Plat*Nmod/NDt PwatTot $=$ PwatTot + Pwat*Nmod/NDt PintTot=PintTot+Pint*Nmod/NDt

RETURN
END
C*********


SUBROUTINE AirOutput

## common variables:


INCLUDE 'type61.inc'
!local variables:
--------------------
REAL Hsat\$,Hrat\$,Habs\$


IF ((IDt.EQ.1).AND. (Itub.EQ.1)) THEN
Tairout $=0$
Hratout=0
END IE
IF (DirAir.NE.O) THEN
!air mix:
Tairout =TairOut + Taix* (Nmod*Saix/SairTot)/NDt
Hratout =Hratout + Hrat* (Nmod*Sair/SairTot)/NDt
IF ((IDt.EQ.NDt).AND. (Itub.EQ.Ntub)) THEN
! condensation of air mix:
HratoutMax=Hrat\$ (Hsat\$ (Tairout), PrAir)
Hratout=MIN (HratOut, HratOutMax)
lother psychometric data:
HabsOut=Habs\$ (HratOut, PrAir)
Hsatout=Hsat\$ (Tairout)
Hrelout $=100$ * HabsOut/Hsatout
END IF

## ELSE

Tairout=TairIn
Hratout=HratIn
HabsOut=HabsIn
Hsatout=Hsatin
HrelOut=Hrelin

END IF
RETURN

SUBROUTINE Soilproperties

```
    !common variables:
```


include 'type6i.inc'

Ssoil (1) $=\mathrm{DY}(\mathrm{J}) * D Z(K)$
Ssoil $(2\rangle=D Y(J) * D Z\langle K)$
IF (I.EQ.1) THEN !border
IF (TYpSOil( $0, \mathrm{~J}, \mathrm{~K}$ ) , EQ. O) THEN tadiabatic
Ksoil $\{1\}=0$
ELSE !surface condition
Ksoil $(1)=1 /(\mathrm{DX}(\mathrm{I}) / 2 /$ LamSoil (TypSois $(\mathbb{I}, \mathcal{J}, \mathrm{K}))$
\&
$+\operatorname{Rsurf}(T y p S o i l(0, J, K))$ )
END IF
ELSE IF (TYpSoil(I-1,J,K).EQ.0) THEN :soil-tube
Ksoil(1) $=0$
ELSE !soil-soil
Ksoil(1) $=2 /(\mathrm{DX}(\mathrm{I}) /$ LamSoil (TypSoil $(\mathrm{I}, \mathrm{J}, \mathrm{K})$ )
$\left.\&_{\text {END IF }}+\operatorname{DX}(I-1) / L a m S o i l(T y p S o i l(I-1, J, K\rangle)\right)$
IF (I.EQ.NJ) THEN !border
IF (TYpSoil (NI +1, J, K).EQ.0) THEN !adiabatic
Ksoil (2) =0
ELSE !surface condition
Ksoil $\{2\}=1 /(\mathrm{DX}(\mathrm{I}) / 2 /$ LamSoil (TYpSoil (I, J, K) )
\&
+ Rsurf(TypSoil(NI+1,J,K)))
END $I F$
ELSE IF (TYpSoil(I+1,J,K).EQ.0) THEN !soil-tube
Ksoil (2) $=0$
ELSE !soil-soil
Ksoil (2) =2/(DX(I)/LamSoil(TypSoil(x, J, K))
\&
END IF
IF (J.EQ.1) THEN ! bordex
Ssoil (3) =DX(I) *DZ (K)
IF (TYpSoil(I, 0,K).EQ.0) THEN !adiabatic
Ksoil $(3)=0$
ELSE !surface condition
Ksoil (3) =1/(DY(J)/2/LamSoil(TypSoil(I,J,K))
\&
+ Rsurf(TypSoil(I, 0,K) ) )
END TF
ELSE IF (TYPSOil(I,J-1,K).EQ.0) THEN !soil-tube
Ssoill (3) $=\mathrm{DX}(\mathrm{X}) * \mathrm{DZ}(\mathrm{K}) *$ CtubCor
Ksoil $(3)=1 /(\operatorname{DY}(J) / 2 /$ LamSoil $($ TypSoil $(I, J, K))+$ ThTub/LamTub $)$
ELSE !SOil-soil
Ssoil(3)=DX(I)*DZ (K)
Ksoil (3) $=2 /(\mathrm{DY}(\mathrm{J}) /$ LamSoil $(T y p S o i l(I, J, K))$
$\left.\hat{E}_{\text {END }} \operatorname{IF}+\operatorname{DY}(J-1) / \operatorname{LamSoil}(\operatorname{TYpSoil}(I, J-1, K))\right)$
IF (J.EQ.NJ) THEN !border
Ssoil (4)=DX(I)*DZ(K)
IF (TYpSoil(I, NJ+I, K).EQ.0) THEN !adiabatic
Ksoil (4)=0
ELSE ! surface condition
Ksoil (4) =1/(DY(J)/2/LamSoil(TypSoil(I, J, K))
+ Rsurf (TypSoil (0, NJ +1, K) ) )
END IF
ELSE IF (TypSoil(I, J+1,K).EQ.0) THEN !soil-tube
Ssoil (4) $=\mathrm{DX}(\mathrm{I}) * \mathrm{DZ}(\mathrm{K}) *$ CtubCor
Ksoil (4) $=1 /(\operatorname{DY}(J) / 2 /$ LamSoil (TYpSoil (I,J,K) $)+$ ThTub/LamTub)
ELSE !soil-soil
Ssoil(4) $=\mathrm{DX}(\mathrm{I}) * \mathrm{DZ}(\mathrm{K})$
Ksoil (4) =2/(DY (J)/LamSoil (TypSoil(I, J, K))
$\&_{\text {END }} I F+D Y(J+1) /$ LamSoil $\left.(\operatorname{TypSoil}(I, J+1, K))\right)$
IF (K.EQ.1) THEN ! border
Ssoil (5) =DX(I) *DY(J)
IF (TYpSoil(I,J,O).EQ.O) THEN !adiabatic
Ksoil $(5)=0$
ELSE !surface condition
Ksoil (5) $=1 /(\mathrm{DZ}(\mathrm{K}) / 2 /$ LamSoil (TypSoil (I, J, K) )
+ Rsur£(TypSoil(I,J,0) ))
END IF
ELSE IF (TYpSoil( $x, J, K-1$ ).EQ.0) THEN !soil-tube

```
            Ssoil(5)=DX(I)*DY(J)*Ctubcor
            Ksoil(5)=1/(DZ(K)/2/LamSoil(TypSoil(I,J,K)) + ThTub/LamTub)
    ELSE !soil-soil
            Ssoil(5)=DX(I)*DY(J)
            Ksoil{5)=2/(DZ(K)/LamSOil{TypSoil(I,J,K))
    & END IF + DZ (K-1)/LamSoil(TypSoil(I,J,K-1))}
        END IF
        IF (K.EQ.NK) THEN !border
        Ssoil(6)=DX(I)*DY(J)
        IF (TypSoil(I,J,NK+1).EQ.O) THEN !adiabatic
            Ksoil{6}=0
        ELSE !surface condition
            Ksoil(6)=1/(DZ (K)/2/LamSoil(TypSoil(I,J,K))
    &
                            + Rsurf(TypSoil(I,J,NK+1)))
        END IF
    ELSE IF (TYpSOil(I,J,K+1).EQ.0) THEN !soil-tube
        Ssoil(6)=DX(I)*DY(J)*CtubCor
        Ksoil(6)=1/(DZ(K)/2/LamSoil(TypSoil(I,J,K)) + ThTub/LamTub)
    ELSE !soil-soil
        Ssoil(6)=DX(I)*DY(J)
        Ksoil(6)=2/(DZ(K)/LamSoil(TypSoil(I,J,K))
    & + DZ(K+1)/LamSoil(TypSoil(\Sigma,J,K+1)))
    END IF
    VolSoil=DX(I)*DY(J)*DZ(K)
    RETURN
    END
**********
c*****************************************************************************
    SUBROUTINE SOilEvolution
    !common variables:
    INCLUDE 'type61.inc'
```



```
    !energy balance :
    Psoil(1)=Ksoil(1)*Ssoil(1)*(Tsoil1(I-1,J,K)-Tsoil1(I,J,K))
    Psoil(2)=Ksoil (2)*Ssoil(2)*(Tsoil1(I+1,J,K)-Tsoil1(I,J,K))
    Psoil(3)=Ksoil(3)*Ssoil(3)*(Tsoill1 (I,J^1,K)-Tsoill(I,J,K))
    Psoil(4)=Ksoil(4)*Ssoil(4)*(Tsoill(I,J+1,K)-Tsoil1(I,J,K))
    Psoil(5)=Ksoil{5)*Ssoil(5)*(Tsoill(I,J,K-1)-Tsoill(I,J,K))
    Psoil(6)=Ksoil(6)*Ssoil(6)*(Tsoill(I,J,K+1)-Tsoil1(I,J,K))
    Psoil(0)=Psoil(1) +Psoil(2)+Psoil(3)+Psoil(4)+Psoil(5)+Psoil(6)
    Pint=Psoil(0)
    Tsoil2(I,J,K)=Tsoill(I,J,K) + Pint*Dt
    &
        /(CvSoil(TypSoil(I,J,K))*VolSoil)
    !integrals :
    !--.---......
    PintTot=PintTot+Pint*Nmod/NDt
    RETURN
    END
C*******************************************************************************
C****************************************************************************
    SUBROUTINE SetBorders
    !common variables:
    !---------------------
    INCLUDE 'type61.inc'
    !local variables:
    !---------------------
    INTEGER Isurf(6)
```



```
    IF (I.EQ.1) THEN
        Isurf(1)=TypSoil(0,J,K)
    ELSE
        Isurf(1)=0
    END IF
    IF (I.EQ.NI) THEN
        Isurf (2)=TypSoil(NI+1,J,K)
    ELSE
        Isurf(2)=0
    END IF
    IF (J.EQ.1) THEN
        Isurf(3)=TypSoil(I,0,K)
    ELSE
        Isurf(3)=0
```

```
```

    END IF
    ```
```

    END IF
    IF (J.EQ.NJ) THEN
    IF (J.EQ.NJ) THEN
        Isurf(4)=TypSoil(I,NJ+1,K)
        Isurf(4)=TypSoil(I,NJ+1,K)
        ELSE
        ELSE
        Isurf(4)=0
        Isurf(4)=0
    END IF
    END IF
    IF (K.EQ.1) THEN
    IF (K.EQ.1) THEN
        Isurf(5)=TypSoi1(I,J,0)
        Isurf(5)=TypSoi1(I,J,0)
    ELSE
    ELSE
        Isurf (5)=0
        Isurf (5)=0
    END IF
    END IF
    IF (K.EQ.NK) THEN
    IF (K.EQ.NK) THEN
        Isurf(6)=TypSoil(I,J,NK+1)
        Isurf(6)=TypSoil(I,J,NK+1)
    ELSE
    ELSE
        Isurf(6)=0
        Isurf(6)=0
    END IF
    END IF
    DO Idir=1,6
    DO Idir=1,6
    IF (Isurf(Idir).GT.0) THEN
    IF (Isurf(Idir).GT.0) THEN
        !set Xbord:
        !set Xbord:
        IF (TypSurf(Isurf(Idir)).EQ.0) THEN !output power:
        IF (TypSurf(Isurf(Idir)).EQ.0) THEN !output power:
            Xbord(Isurf(Iđir)}=Xbord(Isurf(Idir)) + Nmod*Psoil(Idir)/NDt
            Xbord(Isurf(Iđir)}=Xbord(Isurf(Idir)) + Nmod*Psoil(Idir)/NDt
        ELSE IF (IDt.EQ.NDE) THEN !output temperature:
        ELSE IF (IDt.EQ.NDE) THEN !output temperature:
            Xbord(Isurf(Idir))=Xbord(Isurf(Idir))
            Xbord(Isurf(Idir))=Xbord(Isurf(Idir))
            + Tsoil2(I,J,K)*Nmod*Ssoil(Idir)*Ksoil(Idix)
            + Tsoil2(I,J,K)*Nmod*Ssoil(Idir)*Ksoil(Idix)
            /Kbord(Isurf(Idir))/Sbord(Isurf(Idir))
            /Kbord(Isurf(Idir))/Sbord(Isurf(Idir))
        END IF
        END IF
        !set integral:
        !set integral:
        PsurfTot=PsurfTot+Psoil(Idir)*Nmod/NDt
        PsurfTot=PsurfTot+Psoil(Idir)*Nmod/NDt
    END IF
    END IF
    END DO
    END DO
    RETURN
    RETURN
    END
    END
    C*******************************************************************************
C*******************************************************************************
C********************************************************************************
C********************************************************************************
SUBROUTINE SetPhysicalConstants
SUBROUTINE SetPhysicalConstants
!common variables:
!common variables:
!-------------------
!-------------------
INCLUDE 'type61.inc'

```
```

    INCLUDE 'type61.inc'
    ```
```




```
```

        CmAir=1000
    ```
```

        CmAir=1000
        CmWat=4180
        CmWat=4180
        MmolAir=0.0289645
        MmolAir=0.0289645
        MmolWat }=0.018015
        MmolWat }=0.018015
        Rhowat=998
        Rhowat=998
        Clatwat=2501000
        Clatwat=2501000
        CmVap=1805
        CmVap=1805
        Rgas=8.3144
        Rgas=8.3144
    RETURN
    RETURN
    END
    END
    C******************************************************************************
C******************************************************************************
C******************************************************************************
C******************************************************************************
SUBROUTINE OpenParametexFiles
SUBROUTINE OpenParametexFiles
!common variables:
!common variables:
!.-.-n-....--.--------
!.-.-n-....--.--------
!--.~-...-----------

```
```

    !--.~-...-----------
    ```
```




```
```

    INQUYRE (UNIT=IparDEf,OPENED=OparDef)
    ```
```

    INQUYRE (UNIT=IparDEf,OPENED=OparDef)
    IF (.NOT.OparDef) THEN
    IF (.NOT.OparDef) THEN
        OPEN (UNIT=IparDef,FILE='paramdef.txt')
        OPEN (UNIT=IparDef,FILE='paramdef.txt')
    END IF
    END IF
    INQUIRE (UNIT=IparCon,OPENED=OparCon)
    INQUIRE (UNIT=IparCon,OPENED=OparCon)
    IF (.NOT.OparCon) THEN
    IF (.NOT.OparCon) THEN
        OREN (UNIT=IparCon,FILE='paramcon.txt'}
        OREN (UNIT=IparCon,FILE='paramcon.txt'}
    END IF
    END IF
    RETURN
    RETURN
    END
    END
    C******************************************************************************
C******************************************************************************
C*****************************************************************************
C*****************************************************************************
SUBROUTINE ReadSuppliedParameters
SUBROUTINE ReadSuppliedParameters
!common variables:
!common variables:
!-----------------
!-----------------
INCLUDE 'type61.inc'

```
```

    INCLUDE 'type61.inc'
    ```
```




```
    &
```

    &
    1 FORMAT (A)
1 FORMAT (A)
100 FORMAT (12I4)

```
100 FORMAT (12I4)
```

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200 FORMAT (4E12.4)
```

```
GRITE(Iparcon 1)
```

GRITE(Iparcon 1)
WRITE(IparCon,1)'* TYPE 61 SUPPLIED PARAMETERS

```
WRITE(IparCon,1)'* TYPE 61 SUPPLIED PARAMETERS
```




```
!Nmod,Nsec,Nsoil,Nsurf,NT,NJ,NK
```

```
!Nmod,Nsec,Nsoil,Nsurf,NT,NJ,NK
```




```
WRITE(IparCon,1) '* Nmod,Nsec,Nsoil,Nsurf,NI,NJ,NK [-}:'
CALL SkipComment(IparDef)
READ(IparDef,*) Nmod,Nsec,Nsoil,Nsurf,NI,NJ,NK
WRITE(IparCon,100) Nmod,Nsec,Nsoil,Nsurf,NI,NJ,NK
WRITE(IparCon,*)
IF (NmOd.LT.1) CALL StopError(101)
IF (Nsec.LT.1) CALL StopError(102)
IF ((Nsoil.LT.1).OR.(Nsoil.GT.NsoilMax)) CALL StopError(103)
IF ((Nsurf.LT.1).OR.(Nsurf.GT.NsurfMax)) CALE StopError(104)
IF {(NI.LT.1).OR.(NI.GT.NIMax)) CALL StopError(105)
IF ((NJ.LT.2).OR.(NJ.GT.NJMax)) CALL StopError(106)
IF ((NK.LT.3).OR.(NK.GT.NKMax)) CALL StopError(107)
!DX,DY,DZ
WRITE(Iparcon,1) '* DX [m]:'
DX (0)=0
DX (NI +1) =0
CALL SkipComment (IparDef)
READ(IparDef,*) (DX(I),I=1,NI)
WRITE(Iparcon,200) (DX(I),I=1,NI)
WRITE (IparCon,*)
WRITE(IparCon,1) '* DY [m]:'
DY(0)=0
DY (NJ +1) =0
CALL SkipComment(IparDef)
READ(IparDef,*) (DY(J),J=1,NJ)
WRITE(Iparcon,200) (DY(J),J=1,NJ)
WRITE(IparCon,*)
WRITE(IparCon,1) '* DZ [m]:'
DZ (0)=0
DZ (NK+1)=0
CALL SkipComment(IparDef)
READ(IparDef,*) (DZ (K),K=1,NK)
WRITE(IparCon, 200) (DZ (K),K=1,NK)
WRITE(IparCon,*)
DO I=1,NI
    IF (DX(I).LE.0) CALL StopError(201)
END DO
DO J=1,NJ
    IF (DY(J).LE.O) CALL StopError(202)
END DO
DO K=1,NK
    IF (DZ (K).LE.0) CALL StopError(203)
END DO
ITypSec
WRITE(Iparcon,1) '* TypSec [-]:'
CALL SkipComment (IparDef)
READ(IparDef,*) (TypSec(I),I=1,NI)
WRITE(IparCon, 100) (TypSec(I),I=1,NI)
WRITE(IparCon,*)
DO I=1,NI
    IF (TypSec(I).GT.Nsec) CALL StopErxor(301)
END DO
!TypSoil
```



```
DO Isec=0,Nsec+1
    !initialise TypSoil:
    DO J=0,NJ+1
    DO K=0,NK+1
        TypSoil (NIMax,J,K)=0
    END DO
    END DO
    !read TypSoil:
    IF ((Isec.EQ.O).OR.(Isec.EQ.Nsec+1)) THEN
        IF {Isec.EQ.0) THEN
            WRITE(IparCon, FMT='(A32)')
& ** TypSoil for front surface [-]:"
            ELSE
                WRITE(IparCon,FMT='(A31)')
```

```
&
```

\&
END IF
END IF
DO K=1,NK
DO K=1,NK
CALL SkipComment (IparDef)
CALL SkipComment (IparDef)
READ(IparDef,*) (TypSoil(NIMax,J,K),J=1,NJ)
READ(IparDef,*) (TypSoil(NIMax,J,K),J=1,NJ)
WRITE(IparCon,FMT='(4X,60I4)')
WRITE(IparCon,FMT='(4X,60I4)')
(TypSoil(NIMax,J,K),J=1,NJ)
(TypSoil(NIMax,J,K),J=1,NJ)
END DO
END DO
WRITE(IparCon,*)
WRITE(IparCon,*)
ELSE
ELSE
WRITE(IparCon,FMT='(A18,I2,A5)')
WRITE(IparCon,FMT='(A18,I2,A5)')
'* TypSoil for sec\#', Isec,' [-]:'
'* TypSoil for sec\#', Isec,' [-]:'
CALL SkipComment (IparDef)
CALL SkipComment (IparDef)
READ(IparDef,*) (TypSoil(NIMax,J,0),J=1,NJ)
READ(IparDef,*) (TypSoil(NIMax,J,0),J=1,NJ)
WRITE(IparCon,FMT='(4X,60I4)') (TypSoil(NIMax,J,0),J=1,NJ)
WRITE(IparCon,FMT='(4X,60I4)') (TypSoil(NIMax,J,0),J=1,NJ)
DO K=1,NK
DO K=1,NK
CALL SkipComment (IparDef)
CALL SkipComment (IparDef)
READ(IparDef,*) (TypSoil(NIMax,J,K),J=0,NJ+1)
READ(IparDef,*) (TypSoil(NIMax,J,K),J=0,NJ+1)
WRITE(IparCon, FMT='(64I4)')
WRITE(IparCon, FMT='(64I4)')
(TypSoil(NIMax, J, K), J=0,NJ+1)
(TypSoil(NIMax, J, K), J=0,NJ+1)
END DO
END DO
CALL SkipComment (IparDef)
CALL SkipComment (IparDef)
READ(IparDef,*) (TYpSoil(NIMax,J,NK+1),J=1,NJ)
READ(IparDef,*) (TYpSoil(NIMax,J,NK+1),J=1,NJ)
WRITE(IparCon, FMT='(4X,60I4)')
WRITE(IparCon, FMT='(4X,60I4)')
(TypSoil(NIMax,J,NK+1),J=1,NJ
(TypSoil(NIMax,J,NK+1),J=1,NJ
WRITE(IparCon,*)
WRITE(IparCon,*)
END IF
END IF
!test TypSoil:
!test TypSoil:
DO J=0,NJ+1
DO J=0,NJ+1
DO K=0,NK+1
DO K=0,NK+1
IF ((J.GE.1).AND.(J.LE.NJ).AND.(K.GE.1).AND.(K.LE.NK)) THEN
IF ((J.GE.1).AND.(J.LE.NJ).AND.(K.GE.1).AND.(K.LE.NK)) THEN
IF (TypSoil(NIMax,J,K).LT.0) CALL StopError(401)
IF (TypSoil(NIMax,J,K).LT.0) CALL StopError(401)
IF (TypSoil(NIMax,J,K).GT.Nsoil) CALL StopError(402)
IF (TypSoil(NIMax,J,K).GT.Nsoil) CALL StopError(402)
ELSE
ELSE
IF (TypSoil(NIMax,J,K).LT.0) CALL StopError(403)
IF (TypSoil(NIMax,J,K).LT.0) CALL StopError(403)
IF (TypSoil(NIMax,J,K).GT.Nsurf) CALL StopError(404)
IF (TypSoil(NIMax,J,K).GT.Nsurf) CALL StopError(404)
END IF
END IF
END DO
END DO
END DO
END DO
lassign TypSoil:
lassign TypSoil:
IF (Isec.EQ.0) THEN
IF (Isec.EQ.0) THEN
DO J=0,NJ+1
DO J=0,NJ+1
DO K=0,NK+1
DO K=0,NK+1
TypSoil(0,J,K)=TypSoil(NIMax,J,K)
TypSoil(0,J,K)=TypSoil(NIMax,J,K)
END DO
END DO
END DO
END DO
ELSE IF (Isec.EQ.Nsec+1) THEN
ELSE IF (Isec.EQ.Nsec+1) THEN
DO J=0,NJ+1
DO J=0,NJ+1
DO K=0,NK+1
DO K=0,NK+1
TypSoil1(NI+1,J,K)=TypSoil(NIMax, J,K)
TypSoil1(NI+1,J,K)=TypSoil(NIMax, J,K)
END DO
END DO
END DO
END DO
ELSE
ELSE
DO I=1,NI
DO I=1,NI
IF (TypSec(I).EQ.Isec) THEN
IF (TypSec(I).EQ.Isec) THEN
DO J=0,NJ+1
DO J=0,NJ+1
DO K=0,NK+1
DO K=0,NK+1
TypSoil (Y,J,K)=TypSoil (NIMax,J,K)
TypSoil (Y,J,K)=TypSoil (NIMax,J,K)
END DO
END DO
END DO
END DO
END IF
END IF
END DO
END DO
END IF
END IF
END DO
END DO
!test front,back:
!test front,back:
DO J=1,NJ
DO J=1,NJ
DO K=1,NK
DO K=1,NK
IF ((TYpSoil(0,J,K).NE.0}.AND.(TYpSOil(1,J,K).EQ.0))
IF ((TYpSoil(0,J,K).NE.0}.AND.(TYpSOil(1,J,K).EQ.0))
\& CALL StopError(411)
\& CALL StopError(411)
IF ((TypSoil(NI+1,J,K).NE.0).AND. (TypSOil(NI,N,K).EQ.0))
IF ((TypSoil(NI+1,J,K).NE.0).AND. (TypSOil(NI,N,K).EQ.0))
\& CALL StopError(412)
\& CALL StopError(412)
END DO
END DO
END DO
END DO
!test left,right:
!test left,right:
DO I=1,NI
DO I=1,NI
DO K=1,NK
DO K=1,NK
IF (Nmod.EQ.1) THEN
IF (Nmod.EQ.1) THEN
IF (TYpSOI1(I,1,K).EQ.0) CALL StOpError(421)
IF (TYpSOI1(I,1,K).EQ.0) CALL StOpError(421)
IF (TypSoil(I,NJ,K).EQ.0) CALL StopError(422)
IF (TypSoil(I,NJ,K).EQ.0) CALL StopError(422)
IF (TypSoil(I,0,K).NE.0) CONTINUE :423
IF (TypSoil(I,0,K).NE.0) CONTINUE :423
IF (TypSOil(I,NJ+1,K).NE.0) CONTINUE !424
IF (TypSOil(I,NJ+1,K).NE.0) CONTINUE !424
ELSE IF (NmOd.EQ.2) THEN
ELSE IF (NmOd.EQ.2) THEN
IF (TypSoil(I,1,K).EQ.0) CALL StopError(431)
IF (TypSoil(I,1,K).EQ.0) CALL StopError(431)
IF (TypSoil(I,NJ,K).EQ.O) CONTINUE !432

```
            IF (TypSoil(I,NJ,K).EQ.O) CONTINUE !432
```

| 1233 | IF (TypSoil ( $\mathrm{I}, 0, \mathrm{~K}$ ) . NE.0) CONTINUE ! 433 |
| :---: | :---: |
| 1234 | IF (TypSoil (I,NJ+1,K).NE.0) CALL Stoperror(434) |
| 1235 | ELSE |
| 1236 | IF (TypSoil (I,1,K).EQ.0) CONTINUE ! 441 |
| 1237 | IF (TypSoil (I,NJ,K).EQ.0) CONTINUE $: 442$ |
| 1238 | IF (TypSoil ( $1,0, K$ ) .NE.0) CALL Stoperror (443) |
| 1239 | IF (TypSoil( $\mathrm{I}, \mathrm{NJ}+1, \mathrm{~K}$ ) .NE.0) CALL Stoperror(444) |
| 1240 | END IF |
| 1241 | END DO |
| 1242 | END DO |
| 1243 | !test top,bottom: |
| 1244 | DO $\mathrm{I}=1$, NI |
| 1245 | DO $\mathrm{J}=1$, NJ |
| 1246 | IF (TYpSoil(I, J, 1).EQ.0才 CALL Stoperror (451) |
| 1247 | IF (TypSoil(I,J,NK).EQ.0) CALL Stoperror(452) |
| 1248 | END DO |
| 1249 | END DO |
| 1250 |  |
| 1251 | ! PosInf |
| 1252 |  |
| 1253 | WRITE(IparCon, 1) '* PosInf [-]:' |
| 1254 | CALL SkipComment (IparDef) |
| 1255 | READ (Ipardef,*) (Posinf(Ipos), Ipos=1,6) |
| 1256 | WRITE (IparCon, FMT='(6I4)') (PosInf(Ipos), Ipos=1,6) |
| 1257 | WRITE(IparCon,*) |
| 1258 |  |
| 1259 | IF ( $(\operatorname{Posinf}$ (1).LT.1).OR. (PosInf(1).GT.NI)) |
| 1260 | \& CALL Stoperror (501) |
| 1261 | IF ( $(\operatorname{PosInf}(2) . L T .1) . O R .(P o s I n f(2) . G T . N J)) ~$ |
| 1262 | \& CALL Stoperrox (502) |
| 1263 | IF ( $\operatorname{Posinf}(3) . L T$ 1). OR. (PosInf (3).GT.NK)) |
| 1264 | \& CALL Stoperror (503) |
| 1265 | IF ( $($ PosInf (4).LT. PosInf (1)) . OR. (PosInf (4).GT.NI)) |
| 1266 | \& CALL Stoperror (504) |
| 1267 |  |
| 1268 | \& CALL Stoperror(505) |
| 1269 | IF ( $\operatorname{Posinf}(6) . L T \cdot \operatorname{Posinf}(3))$. OR. (PosInf (6).GT.NK) $)$ |
| 1270 | \& CALL Stoperror(506) |
| 1271 |  |
| 1272 | ! Kair0, Kair1 |
| 1273 |  |
| 1274 | WRITE(IparCon,1) '* Kairo [kJ/hr K m2]' |
| 1275 | \& $\quad$, Kair1 [(kJ/hr K m2)/(m/s)]:' |
| 1276 | CALL SkipComment (IparDef) |
| 1277 | READ(IparDef,*) Kair0, Kair1 |
| 1278 | WRITE(IparCon, 200) Kair0,KairI |
| 1279 | WRITE(IparCon,*) |
| 1280 ( |  |
| 1281 | IF ((Kair0.LT.0).OR. (Kair1.LT.0)) CALL StopError (601) |
| 1282 | Kair0 Kair0/3.6 ! [W/K m2] <- [kJ/hr K m2] |
| 1283 | Kairl=Kairl/3.6 : $[(\mathrm{W} / \mathrm{K} \mathrm{m} 2) /(\mathrm{m} / \mathrm{s})]<-[(\mathrm{kJ} / \mathrm{hx} \mathrm{K} \mathrm{m2}) /(\mathrm{m} / \mathrm{s})]$ |
| 1284 ( $12{ }^{\text {a }}$ |  |
| 1285 | LLamSoil, CvSoil |
| 1286 !--------......... |  |
| 1287 | WRITE(IparCon,1) '* LamSoil [ $\mathrm{kJ} / \mathrm{hrx} \mathrm{Km}$ ], CvSoil [ $\mathrm{kJ} / \mathrm{K} \mathrm{m} 3]:$ ' |
| 1288 | DO Isoill=1,Nsoil |
| 1289 | CALL SkipComment (IparDef) |
| 1290 | READ (IparDef, *) LamSoil (Isoil), CvSoil (Isoil) |
| 1291 | WRITE(IparCon, 200) LamSoil (Isoil), CvSoil (Isoil) |
| 1292 | END DO |
| 1293 | WRITE (Iparcon, *) |
| 1294 ( 1 |  |
| 1295 | DO Isoil $=1$, Nsoil |
| 1296 | IF (LamSoil(Isoil). LE.0) CALL StopError(701) |
| 1297 | IF (CvSoil(Isoil). LE.0) CALL Stoperror (702) |
| 1298 | LamSoil(Isoil)=LamSoil (Isoil)/3.6 ! [w/ Km ] $<-[\mathrm{kJ} / \mathrm{hr} \mathrm{K} \mathrm{m]}$ |
| 1299 |  |
| 1300 | END DO |
| 1301 |  |
| 1302 | ! LamTub, CvTub |
|  |  |
| 1304 | WRITE(IparCon,1) '* LamTub [kJ/hx K m], CvTub [kJ/K m3]:' |
| 1305 | CALL SkipComment (IparDef) |
| 1306 | READ (IparDef,*) LamTub, CvTub |
| 1307 | WRITE(IparCon, 200) LamTub, CvTub |
| 1308 | WRITE(IparCon,*) |
| 1309 ( 1308 |  |
| 1310 | IF (LamTub.LE.0) CALL Stoperror (801) |
| 1311 | IF (CvTub. Le.0) CALL Stoperror (802) |
| 1312 | LamTub=LamTub/3.6 ! [W/K m] <- [kJ/hr K m] |
| 1313 | CvTub=CvTub*1000 ! [J/K m3] <n [kJ/K m3] |
| 1314 l |  |
| 1315 | fThTub, Ctubcor, Rexic |
| 1316 |  |
| 1317 | WRITE(IparCon,1) '* ThTub [m], CtubCor [-], Rfric [-]:' |
| 1318 | CALL SkipComment(IparDef) |
| 1319 | READ (IparDef,*) ThTub, CtubCor, Rfric |
| 1320 | WRITE(Iparcon, 200) ThTub, CtubCor, Rfric |

```
WRITE(IparCon,*)
```

WRITE(IparCon,*)
IF (ThTub.LT.0) CALL StopError(901)
IF (CtubCor.LE.0) CALL StopError(902)
IF (Rfric.LT.0) CALL StopError(903)
!TypWat, Vwat
WRITE(IparCon,1) '* TypWat [-], Vwat [m/hr]:
CALL SkipComment(IparDef)
READ(IparDef,*) (TypWat(Idix),Idir=-1,1)
WRITE(IparCon,100} (TypWat(Idir},Idir=-1,1)
CALL SkipComment(IparDef)
READ(IparDef,*) (Vwat(Idir),Idix=-1,1)
WRITE(IpaxCon,200) (Vwat(Idir),Idir=-1,1)
WRITE(IparCon,*)
DO Idir=-1,1
IF ((TypWat(Idir).LT.1).OR.(TypWat(Idir).GT.2))
\& CALL StopErrox(1001)
IF (Vwat(Idir).LT.O) CALL StopError(1002)
Vwat (Idir)=Vwat(Idir)/3600 ! [m/s] < [m/hr]
END DO
NNiniSoil,NiniWat
WRITE(IparCon,1) '* NiniSoil,NiniWat [-]:'
CALL SkipComment(IparDef)
READ(IparDef,*) NiniSoil,NiniWat
WRITE(IparCon,100) NiniSoil,NiniWat
WRITE(IparCon,*)
IF ((NiniSOil.LT.1).OR.(NiniSoil.GT.NiniMax)) CALI StopErrox(1101)
IF ((NiniWat.LT.1).OR.(NiniWat.GT.NiniMax)) CALL StopError(1102)
!TiniSoil, PosIniSoil
WRITE(Iparcon,1) '* TiniSoil [degC], PosIniSoil [-]:'
CALL SkipComment (IparDef)
READ(IparDef,*) TiniSoil(1)
WRITE(IparCon,200) TiniSoil(1)
DO Iini=2,NiniSoil
CALL SkipComment(IparDef)
READ(IparDef,*) TiniSoil(Iini),(PosIniSoil(Iini,Ipos),Ipos=1,6)
WRITE(IparCon,FMT='(E12.4,6I4)')
\&
TiniSoil(Iini),(PosIniSoil(Iini,Ipos),Ipos=1,6)
END DO
WRITE(IparCon,*)
DO Iini=2,NiniSoil
IF ((POsIniSoil(Iini,1).LT.1).OR. (PosIniSoil(Iini,1).GT.NI))
\& CALL StopError(1201)
IF ((POSIniSoil(IIni,2).LT.1).OR.(POSIniSoil(Iini,2).GT.NJ))
\& CALL StopError(1202)
IF ((POSIniSoil(IIni,3).ET.1).OR.(POSIniSoil(Iini,3).GT.NK))
\& CALL StopError(1203)
IF ((PosIniSoil(Iini,4).LT.PosIniSoil(Iini,1)).OR.
\& (PosIniSoil(Iini,4).GT.NI)) CALL StopError(1204)
IF ((POSIniSoil(INni,5).LT.POSIniSoil(IIni,2)).OR.
\& (PosIniSoil(Iini,5).GT.NJ)) CALL StopError(1205)
IF ((POSIniSoil(INMi,6).LT.POSIniSoil(IIni,3)).OR.
\& (PosIniSoil(Iini,6).GT.NK)) CALL StopError(1206)
END DO
!ThIniWat, PosIniWat
WRITE(IparCon,1) '* ThIniWat [m], PosIniWat [.-]:
CALL SkipComment (IparDef)
READ(IparDef,*) ThIniWat(1)
WRITE(IpaxCon, 200) ThIniWat(1)
DO Iini=2,NiniWat
CALL SkipComment (IparDef)
READ(IparDef,*) ThIniWat(Iini),(PosIniWat(IIni,Ipos), Ipos=1,6)
WRITE(IparCon,FMT='(E12.4,6I4)')
\& ThIniWat(Iini),(PosIniWat(IIni,Ipos),Ipos=1,6)
END DO
WRITE(IparCon,*)
DO Iini=2,NiniWat
IF ({POSIniWat(Ini,1).LT.1).OR.(PosIniWat(Iini,1).GT.NI))
\& CALL StopError(1301)
IF ((POSIniWat(Iini,2).LT.1).OR. (POSIniWat(Iini,2).GT.NJ))
\& CALL StOpError(1302)
IF ({POsIniWat(IIni,3).LT.1).OR. (PosIniWat(IIni, 3).GT.NK)}
\& CALL StopError(1303)
IF ((PosIniWat (IIni,4).LT. PosIniWat(IIni,1)).OR.
\& (PosIniWat(Iini,4).GT.NI)) CALL StopError(1304)
IF ((PosIniWat(Iini,5).LT.PosIniWat(Iini,2)).OR.

```

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```
                IflowIni=I
```

                IflowIni=I
            END IF
            END IF
            IF (I.GT.IflowEnd) THEN
            IF (I.GT.IflowEnd) THEN
                If lowEnd=I
                If lowEnd=I
            END IF
            END IF
        END IF
        END IF
    END DO
END DO
WRITE(IparCon, FMT='(A11,14X,I4)') '* Ntub [~]:',Ntub
WRITE(IparCon, FMT='(A11,14X,I4)') '* Ntub [~]:',Ntub
WRITE(IparCon,FMT ='(A15,10X,I4)') '* IflowIni [-1:',IflowIni
WRITE(IparCon,FMT ='(A15,10X,I4)') '* IflowIni [-1:',IflowIni
WRITE(IparCon,FMT='(A15,10X,I4)') '* IflowEnd [-]:',IflowEnd
WRITE(IparCon,FMT='(A15,10X,I4)') '* IflowEnd [-]:',IflowEnd
IF (Ntub.GT.NtubMax) CALL StopError(2101)
IF (Ntub.GT.NtubMax) CALL StopError(2101)
!PosTub
!PosTub
!test tube compatibility between sections:
!test tube compatibility between sections:
DO I=IflowIni+1, IflowEnd
DO I=IflowIni+1, IflowEnd
DO J=1,NJ
DO J=1,NJ
DO K=1,NK
DO K=1,NK
TF(
TF(
\& ((TypSoil(I,J,K).EQ.0).AND.(TypSoil(IflowIni,J,K).NE.0))
\& ((TypSoil(I,J,K).EQ.0).AND.(TypSoil(IflowIni,J,K).NE.0))
\& .OR.
\& .OR.
\& ((TypSoil(I,J,K).NE.0).AND.(TYpSoil(IflowIni,J,K).EQ.0))
\& ((TypSoil(I,J,K).NE.0).AND.(TYpSoil(IflowIni,J,K).EQ.0))
\& ) CALL StopError(2201)
\& ) CALL StopError(2201)
END DO
END DO
END DO
END DO
END DO
END DO
!set PosTub:
!set PosTub:
xtub=0
xtub=0
DO }J=1,N
DO }J=1,N
DO K=1,NK
DO K=1,NK
IF (TYpSoil(IEIOWIni,J,K).EQ.0) THEN
IF (TYpSoil(IEIOWIni,J,K).EQ.0) THEN
Itub=Itub+1
Itub=Itub+1
PosTub(Itub,1)=J
PosTub(Itub,1)=J
PosTub(Itub, 2)=K
PosTub(Itub, 2)=K
END IF
END IF
END DO
END DO
END DO
END DO
DO Itub=1,Ntub
DO Itub=1,Ntub
WRITE(IparCon, FMT='(A10,I2,A5, 8X, 2I4)')
WRITE(IparCon, FMT='(A10,I2,A5, 8X, 2I4)')
\& '* PosTub \#', xtub,' [-]:',PosTub(Itub,1), PosTub(Itub,2)
\& '* PosTub \#', xtub,' [-]:',PosTub(Itub,1), PosTub(Itub,2)
END DO
END DO
!LX, LY,LZ,Ltub

```
!LX, LY,LZ,Ltub
```




```
LX=0
```

LX=0
DO I=1,NI
DO I=1,NI
LX=LX+DX(I)
LX=LX+DX(I)
END DO
END DO
WRITE(IparCon, FMT='(A9,16X,E12.4)') '* LX [m]:',LX
WRITE(IparCon, FMT='(A9,16X,E12.4)') '* LX [m]:',LX
LY=0
LY=0
DO J=1,NJ
DO J=1,NJ
LY=LY+DY(J)*Nmod
LY=LY+DY(J)*Nmod
END DO
END DO
WRITE(IparCon,FMT='(A9,16X,E12.4)') '* LY {m}:',LY
WRITE(IparCon,FMT='(A9,16X,E12.4)') '* LY {m}:',LY
LZ=0
LZ=0
DO K=1,NK
DO K=1,NK
LZ=LZ+DZ(K)
LZ=LZ+DZ(K)
END DO
END DO
WRITE(IparCon,FMT='(A9,16X,E12.4)') '* LZ [m]:',LZ
WRITE(IparCon,FMT='(A9,16X,E12.4)') '* LZ [m]:',LZ
Ltub=0
Ltub=0
DO I=IflowIni,IflowEnd
DO I=IflowIni,IflowEnd
Ltub=Ltub+DX(I)
Ltub=Ltub+DX(I)
END DO
END DO
WRITE(IparCon,FMT='(A11,14X,E12.4)') '* Ltub (m]:',Ltub
WRITE(IparCon,FMT='(A11,14X,E12.4)') '* Ltub (m]:',Ltub
!SairTot,StubTot,ZairTot
!SairTot,StubTot,ZairTot
!--------------------.----------------...--------------------------------------
!--------------------.----------------...--------------------------------------
SairTot=0
SairTot=0
StubTot=0
StubTot=0
DO Itub=1,Ntub
DO Itub=1,Ntub
Iflow=IflowIni
Iflow=IflowIni
CALL TubeProperties
CALL TubeProperties
SairTot=SairTot + Sair*Nmod
SairTot=SairTot + Sair*Nmod
StubTot=StubTot + Stub*Nmod*Ltub/DX(I)
StubTot=StubTot + Stub*Nmod*Ltub/DX(I)
ZairTot=ZairTot + Zair*Nmod
ZairTot=ZairTot + Zair*Nmod
END DO
END DO
WRITE(IparCon,FMT='(A15,10X,E12.4)') '* SairTot [m2]:',SairTot
WRITE(IparCon,FMT='(A15,10X,E12.4)') '* SairTot [m2]:',SairTot
WRITE(IparCon, FMT='(A15,10X,E12.4)') '* StubTot [m2]:',StubTot
WRITE(IparCon, FMT='(A15,10X,E12.4)') '* StubTot [m2]:',StubTot
WRITE(IparCon,FMT='(A17,8X,E12.4)') '* ZairTot [m5/2]:',ZairTot
WRITE(IparCon,FMT='(A17,8X,E12.4)') '* ZairTot [m5/2]:',ZairTot
SSinfTot
SSinfTot
!--------.-.--------------------------------------------------------------------

```
!--------.-.--------------------------------------------------------------------
```

| 1585 | Sinftot $=0$ |
| :---: | :---: |
| 1586 | DO Itub=1, Ntub |
| 1587 | DO I=Iflowini, Iflowend |
| 1588 | CALL TubeProperties |
| 1589 | IF ((I.GE.PosInf(1)).AND.(I.LE.PosInf(4))) THEN |
| 1590 | IF ((J.GE.PosInf(2)). AND. (J.LE.POSInf(5))) THEN |
| 1591 | IF ( $\mathrm{K} . \mathrm{GE} . \operatorname{Posinf}(3)$ ).AND. (K.LE.POsInf(6) ) ) THEN |
| 1592 | SinfTot=SinfTot + Stub*Nmod |
| 1593 | END IF |
| 1594 | END IF |
| 1595 | END IF |
| 1596 | END DO |
| 1597 | END DO |
| 1598 | WRITE(IparCon, FMT = '(A15,10X, E12.4)') '* Sinftot [m2):', Sinftot |
| 1599 |  |
| 1600 | ! Sbord |
| 1601 | !- |
| 1602 | ! set Sbord: |
| 1603 | Sbord $=0$ |
| 1604 |  |
| 1605 | DO $I=1, N \mathrm{~N}$ |
| 1606 | DO $\mathrm{J}=1$, NJ |
| 1607 | Isurf=TypSoil ( $1, J, 0$ ) |
| 1608 | IF (Isurf.GT.0) Sbord(Isurf) $=$ Sbord(Isurf) + DX (I) *DY(J) *Nmod |
| 1609 | Isurf=TypSoil(I, J,NK+1) |
| 1610 | IF (Isurf.GT.0) Sbord(Isurf) =Sbord(Isurf) $+\mathrm{DX}(\mathrm{I}) * \mathrm{DY}(\mathrm{J}) * \mathrm{Nmod}$ |
| 1611 | END DO |
| 1612 | END DO |
| 1613 |  |
| 1614 | DO $\mathrm{I}=1, \mathrm{NI}$ |
| 1615 | DO K=1,NK |
| 1616 | Isurf $=$ TypSoil (I, 0, K) |
| 1617 | IF (Isurf.GT.0) Sbord(Isurf) = Sbord(Isurf) $+\mathrm{DX}(\mathrm{I}) * \mathrm{DZ}$ (K) *Nmod |
| 1618 | Isurf=TypSoil ( $\mathrm{I}, \mathrm{NJ}+1, \mathrm{~K}$ ) |
| 1619 | IF (Isurf.GT.0) Sbord(Isurf) $=$ Sbord(Isurf) $+\mathrm{DX}(\mathrm{I}) * \mathrm{DZ}(\mathrm{K}) * \mathrm{Nmod}$ |
| 1620 | END DO |
| 1621 | END DO |
| 1622 |  |
| 1623 | DO $\mathrm{J}=1$, NJ |
| 1624 | DO $\mathrm{K}=1$, NK |
| 1625 | Isurf=TypSoil (0, J, K) |
| 1626 |  |
| 1627 | Isurf=TypSoil ( $\mathrm{NI}+1, \mathrm{~J}, \mathrm{~K}$ ) |
| 1628 | IF (Isurf.GT.0) Sbord(Isurf) $=$ Sbord(Isurf) $+\mathrm{DY}(\mathrm{J}) * \mathrm{DZ}$ (K) *Nmod |
| 1629 | END DO |
| 1630 | END DO |
| 1631 |  |
| 1632 | DO Isurf=1, Nsurf |
| 1633 | WRITE (IparCon, FMT = ' (A9, I2, A6, 8X, E12.4)') |
| 1634 | \& '* Sbord \#', Isurf,' \{m2\}:', Sbord(Isurf) |
| 1635 | END DO |
| 1636 |  |
| 1637 | ! Kbord |
| 1638 |  |
| 1639 | ! set Kbord: |
| 1640 | Kbord=0 |
| 1641 |  |
| 1642 | DO $\mathrm{I}=1$, NI |
| 1643 | DO $J=1$, NJ |
| 1644 | Isurf=TypSoil (I, J, O) |
| 1645 | IF (Isurf.GT.0) Kbord(Isurf) $=$ Kbord(Isurf) + DX(I)*DY(J)*Nmod |
| 1646 | \& *2*LamSoil (TypSoil (I, J, 1) )/DZ (1) |
| 1647 | Isurf=TypSoil( $1, \pm, N \mathrm{~N}+1$ ) |
| 1648 | IF (Isuxf.GT.0) Kbord(Isurf) $=$ Kbord(Isurf) $+\mathrm{DX}(\mathrm{I}) * D Y(J) * N m o d$ |
| 1649 | \& *2*LamSoil (TypSoil (Y, J, NK) )/DZ (NK) |
| 1650 | END DO |
| 1651 | END DO |
| 1652 |  |
| 1653 | DO $\mathrm{I}=1, \mathrm{NI}$ |
| 1654 | DO $\mathrm{K}=1$, NK |
| 1655 | Isurf=TypSoil (I, 0, K) |
| 1656 | IF (Isurf.GT.0) Kbord(Isurf) =Kbord(Isurf) $+\mathrm{DX}(\mathrm{I}) * \mathrm{DZ}$ (K) *Nmod |
| 1657 | \& *2*LamSoil(TypSoil(I, 1, K) )/DY(1) |
| 1658 | Isurf=TYpSoil (I, $\mathrm{NJ}+1, \mathrm{~K}$ ) |
| 1659 | IF (Isurf.GT.0) Kbord(Isurf) $=$ Kbord(Isurf) $+\mathrm{DX}(\mathrm{I}) * \mathrm{DZ}(\mathrm{K}) *$ Nmod |
| 1660 | \& *2*LamSoil (TypSoil (I, NJ, K) )/DY (NJ) |
| 1661 | END DO |
| 1662 | END DO |
| 1663 |  |
| 1664 | DO $\mathrm{J}=1$, NJ |
| 1665 | DO K=1, NK |
| 1666 | Isurf =TypSoil (0,J,K) |
| 1667 | IF (Isuxf.GT.0) Kbord(Isurf) $=$ Kbord(Isurf) $+\mathrm{DY}(\mathrm{J}) * \mathrm{DZ}(\mathrm{K}) * \mathrm{Nmod}$ |
| 1668 | \& *2*LamSoil (TypSoil (1, J, K) )/DX(1) |
| 1669 | Isurf=TypSoil (NI+1,J,K) |
| 1670 | IF (Isurf.GT.0) Kbord(Isurf) =Kbord(Isurf) $+\mathrm{DY}(\mathrm{J}) * \mathrm{DZ}(\mathrm{K}) * \mathrm{Nmod}$ |
| 1671 | \& *2*LamSoil (PYpSoil (NI, J, K) )/DX(NI) |
| 1672 | END DO |

END DO
DO Isurf=1, Nsurf
IF (Sbord(Isurf).EQ.O) THEN Kbord $($ Isurf $)=0$
ELSE
Kbord(Isurf) $=$ Kbord(Isurf)/Sbord(Isure)
END IF
END DO
DO Isurf $=1$, Nsurf
WRITE (IparCon, FMT=' (A9, I2, A12, 2X, E12.4)')
\& ** Kbord \#', Isurf,' [kJ/hr K m2]:', Kbord(Isuxf)*3.6 ! [kJ/hr K m2] <- [W/K m2] END DO
! DtSoil, DtWat
!set DtSoil:
Ncount $=0$
DtSoil=0
DO $I=1$,NI
DO $J=1, N J$
DO $K=1$, NK
IF (TypSoil(I,J,K).NE.0) THEN
Ncount $=$ Ncount +1
CALL SoilProperties
DtIJK=CVSoil(TypSoil (I, J, K))*VolSoil/2
$\& \quad /($ Ksoil (1)*Ssoil(1) +Ksoil (2)*Ssoil (2) + Ksoil (3)*Ssoil (3)
$\& \quad+\mathrm{Ksoil}(4) * \operatorname{ssoil}(4)+\mathrm{Ksoil}(5) * \operatorname{ssoil}(5)+\mathrm{Ksoil}(6) * \operatorname{ssoil}(6)$
IF (Ncount.EQ.1) THEN
DtSoil=DtIJK
ELSE
DtSoil=MIN(DtSoil, DtIJK)

## END IF

END IF
END DO
END DO
END DO
WRITE (IparCon, FMT='(A14,11X,E12.4)') '* DtSoil [hr]: *, 3600*DtSoil ! [hr] <- [s]
!set DtWat:
Ncount=0
DtWat $=0$
DO Idir=-1,1
IF ((TypWat(Idir).EQ.1).AND. (Vwat(Idix).GT.0)) THEN
DO I=IflowIni, IflowEnd
Ncount $=$ Ncount +1
DtIJK=DX (I)/Vwat (Idir)
IF (Ncount.EQ.1) THEN
DtWat $=$ DtIJK
ELSE
Dtwat =MIN (DtWat, DtIJK)
END IF
END DO
END IF
END DO
IF (DtWat.GT.0) THEN
WRITE (IparCon, FMT = ' $\left.\langle\mathrm{A} 13,12 \mathrm{X}, \mathrm{E} 12,4)^{\prime}\right\rangle$ ** DtWat [hr):',3600*DtWat ! [hr] <- [s] ELSE

WRITE (IparCon, FMT='(A13,14X,A4)') '* DtWat [hr]:','none'
END IF
! FairMinTub
! set FairMinTub
Ncount=0
FairMinTub=0
DO Itub=1, Ntub
DO Iflow $=$ Iflowini, IflowEnd
Ncount=Ncount +1
CALL Tubeproperties
FairMinIJK=2*SairTot*Stub*Kair0/(Sair*1290-2*Stub*Kair1)
! (air capacity at normal condition: $1290 \mathrm{~J} / \mathrm{K} / \mathrm{m} 3$ )
IF (Ncount.EQ.1) THEN
FairMinTub=FairMinIJK
ELSE
FairMinTub=MIN (FairMinIJK, FairMinTub)
END IF
END DO
END DO
WRITE (IparCon, FMT = ' (A21, 4X, E12. 4)')
\&'* FairMinTub [m3/hr]:',3600*FairMinTub ! [m3/hr]<- [m3/s]

```
WRITE(IparCon, 1)'***************************************************
```

WRITE (IparCon, *)

RETURN
END

```
C*******************************************************************************
```

C*******************************************************************************
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```
***********************************************************************
```

***********************************************************************
SUBROUTINE SetSimulationParameters
SUBROUTINE SetSimulationParameters
!common variables:
!common variables:
cornon variables.
cornon variables.
REAL TIMEO,TIMEF,DELT,IWARN
REAL TIMEO,TIMEF,DELT,IWARN
COMMON /SIM/ TIMEO,TIMEF,DELT,IWARN
COMMON /SIM/ TIMEO,TIMEF,DELT,IWARN
INCLUDE 'type61.inc

```
    INCLUDE 'type61.inc
```




```
FORMAT (A)
```

FORMAT (A)
WRITE(IparCon, 1);****************************************************
WRITE(IparCon, 1);****************************************************
WRITE(IparCon,1)'* TYPE 61 SIMULATION PARAMETERS

```
    WRITE(IparCon,1)'* TYPE 61 SIMULATION PARAMETERS
```




```
    !simulation timestep:
```

    !simulation timestep:
    IF (DE.EQ.0) THEN
    IF (DE.EQ.0) THEN
        IF (DtWat.EQ.0) THEN
        IF (DtWat.EQ.0) THEN
            NDt=MAX(IFIX{3600*DELT/DtSoil},1)
            NDt=MAX(IFIX{3600*DELT/DtSoil},1)
        ELSE
        ELSE
            NDt=MAX(IFIX{3600*DELT/MIN(DtSoil,DtWat)),1)
            NDt=MAX(IFIX{3600*DELT/MIN(DtSoil,DtWat)),1)
        END IF
        END IF
        ELSE
        ELSE
        NDt=MAX(IFIX(3600*DELT/Dt),1)
        NDt=MAX(IFIX(3600*DELT/Dt),1)
        END IF
        END IF
    Dt =3600*DELT/NDt
    Dt =3600*DELT/NDt
    WRITE(IparCon,FMT='(A10,15X,E12.4)') '* Dt [hr]:',Dt/3600 ! [hr] <- [s]
    WRITE(IparCon,FMT='(A10,15X,E12.4)') '* Dt [hr]:',Dt/3600 ! [hr] <- [s]
    mminimal aixflow:
    mminimal aixflow:
    IF (FairMin.EQ.0) THEN
    IF (FairMin.EQ.0) THEN
        FairMin=FaixMinTub
        FairMin=FaixMinTub
    END IF
    END IF
    WRITE(IparCon,FMT='(A18,7X,E12.4)') '* FairMin [m3/hr]:'
    WRITE(IparCon,FMT='(A18,7X,E12.4)') '* FairMin [m3/hr]:'
    &
    &
    WRITE(IparCon,1)
    WRITE(IparCon,1)
    WRITE(***)
    WRITE(***)
    RETURN
    RETURN
    END
    END
    C*******************************************************************************
C*******************************************************************************
C*****************************************************************************
C*****************************************************************************
SUBROUTINE CloseParameterFiles
SUBROUTINE CloseParameterFiles
!common variables:
!common variables:
INCLUDE

```
    INCLUDE
```




```
    IF (.NOT.OparDef) THEN
```

    IF (.NOT.OparDef) THEN
        CLOSE (IparDef
        CLOSE (IparDef
    END IF
    END IF
    IF (.NOT.OparCon) THEN
    IF (.NOT.OparCon) THEN
        ClOSE (Iparcon)
        ClOSE (Iparcon)
    END IF
    END IF
    RETURN
    RETURN
    END
    END
    C******************************************************************************
C******************************************************************************
C*******************************************************************************
C*******************************************************************************
SUBROUTINE InitialiseSoil
SUBROUTINE InitialiseSoil
!common variables:
!common variables:
!---------------------
!---------------------
INCLUDE 'type61.inc'

```
    INCLUDE 'type61.inc'
```




```
    DO I=1,NI
```

    DO I=1,NI
    DO J=1,NJ
    DO J=1,NJ
    DO K=1,NK
    DO K=1,NK
        Tsoil0(I,J,K)=TiniSoil(I)
        Tsoil0(I,J,K)=TiniSoil(I)
        Tsoill(I,J,K)=TiniSoil(1)
        Tsoill(I,J,K)=TiniSoil(1)
        Tsoi12(I,J,K)=TiniSoil(1)
        Tsoi12(I,J,K)=TiniSoil(1)
        END DO
        END DO
        END DO
        END DO
        END DO
        END DO
        DO Iini=2,NiniSoil
        DO Iini=2,NiniSoil
        DO I=PosIniSoil(Iini,1), PosIniSoil(Iini,4)
        DO I=PosIniSoil(Iini,1), PosIniSoil(Iini,4)
        DO J=PosIniSoil(Iini, 2), PosIniSoil(Iini,5)
        DO J=PosIniSoil(Iini, 2), PosIniSoil(Iini,5)
        DO K=PosIniSoil(Iini,3), PosIniSoil(Iini,6)
        DO K=PosIniSoil(Iini,3), PosIniSoil(Iini,6)
        Tsoilo(I,J,K)=TiniSoil(In_i)
        Tsoilo(I,J,K)=TiniSoil(In_i)
        Tsoill(I,J,K)=TiniSoil(Iini)
    ```
        Tsoill(I,J,K)=TiniSoil(Iini)
```

```
            Tsoil2(I,J,K)=TiniSoil(INEi)
    END DO
    END DO
    END DO
    END DO
    RETURN
    END
C*******************************************************************************
C*******************************************************************************
    SUBROUTINE InitialiseWater
    !common variables:
    !---------...--..--------
    INCmuDE Cype61.inc
```



```
    DO Itub=1,Ntub
    DO Iflow=IflowIni,IflowEnd
        CALL TubeProperties
        Mwat0(Iflow, Itub)=Stub*ThIniWat (1)*Rhowat
        Mwat1 (Iflow, Itub)=Stub*ThIniWat (1)*RhoWat
        Mwat2{Iflow,Itub} =Stub*ThIniWat (1)*RhoWat
        END DO
    END DO
    DO Iini=2,NiniWat
    DO Itub=1,Ntub
    DO Iflow=IflowIni,IflowEnd
        CALL TubeProperties
        IF ((I.GE.PosIniWat(Iini,1)).AND.(I.LE.POSIniWat(Iini,4))) THEN
        IF ((J.GE.PosIniWat(Iini,2)).AND.(J.LE.PosIniWat(Iini,5))) THEN
        IF ((K.GE.POSIniWat(Iini,3)).AND. (K.LE.PosIniWat(IIni,6))) THEN
            Mwat0(I,Itub)=Stub*ThIniWat (Iini)*RhoWat
            Mwat1(I, Itub)=Stub*ThIniWat (İni)*Rhowat
            Mwat2 (I,Itub)=Stub*ThIniWat(Iini)*RhoWat
            END IF
            END IF
            END IF
        END DO
    END DO
    END DO
    RETURN
    END
C*****************************************************************************
C******************************************************************************
    SUBROUTINE OptionalsTube
    !common variables:
    !-.---.-------------
    llocal variables:
    INTEGER Ipos,Jpos,Kpos,NnodeOpt (NoptMax)
```



```
    IInitialise NnodeOpt:
    !----m----------------
    IF (Isim.LT.3) THEN
    IF (IDt.EQ.1) THEN
    IF ((Itub.EQ.1).AND.(Iflow.EQ.IflowIni)) THEN
    DO Iopt=1, Nopt
        IF (INT(TypOpt(Iopt)/100).EQ.0) THEN
            NnodeOpt(Iopt)=0
            DO Ipos=POSOpt (Iopt, 1), PosOpt (IOpt,4)
            DO Jpos=POSOpt(IOpt, 2), PosOpt(IOpt, 5)
            DO Kpos=PosOpt(Iopt, 3), PosOpt(Iopt,6)
            IF {TypSoil(Ipos,Jpos,Kpos).EQ.0} THEN
                    NnodeOpt (Iopt)=NnodeOpt (Iopt) +1
            END IF
            END DO
            END DO
                END DO
            END IF
    END DO
    END IF
    END IF
    END IF
    !Update Opt:
    !---------------
    DO Iopt=1,Nopt
    IF (INT (TypOpt(IOpt)/100).EQ.0) THEN
    IF ((I.GE. PosOpt (Iopt, 1)).AND. (I.LE.POSOpt(Iopt,4))) THEN
```



```
            !Psoil(6) [kJ/hr]
```

            !Psoil(6) [kJ/hr]
            Opt(IOpt)=Opt(IOpt)+Psoil(6)*3.6*Nmod/NDt
            Opt(IOpt)=Opt(IOpt)+Psoil(6)*3.6*Nmod/NDt
            GOTO 999
            GOTO 999
            !Pint [kJ/hx]
            !Pint [kJ/hx]
            Opt (Iopt)=Opt (Iopt) +Pint* 3.6*Nmod/NDt
            Opt (Iopt)=Opt (Iopt) +Pint* 3.6*Nmod/NDt
            GOTO 999
            GOTO 999
            !Fair [m3/hr]
            !Fair [m3/hr]
            IF (Iflow.EQ.IflowIni)
            IF (Iflow.EQ.IflowIni)
            Opt(Iopt)=Opt(Iopt) +Fair* 3600/NnodeOpt (Iopt)/NDt
            Opt(Iopt)=Opt(Iopt) +Fair* 3600/NnodeOpt (Iopt)/NDt
            GOTO 999
            GOTO 999
            !Vair [m/s]
            !Vair [m/s]
            IF (Iflow.EQ.IflowIni)
            IF (Iflow.EQ.IflowIni)
            Opt(Iopt)=Opt(Iopt)+Vair/NnodeOpt(Iopt)/NDt
            Opt(Iopt)=Opt(Iopt)+Vair/NnodeOpt(Iopt)/NDt
                    GOTO }99
                    GOTO }99
                    CONTINUE
                    CONTINUE
            END IF
            END IF
            END IF
            END IF
            END IF
            END IF
            END IF
            END IF
            END DO
            END DO
            RETURN
            RETURN
            END
            END
    C*****************************************************************************
C*****************************************************************************
C******************************************************************************
C******************************************************************************
SUBROUTINE OptionalsSoil
SUBROUTINE OptionalsSoil
!common variables:
!common variables:
!---no----
!---no----
INCLUDE 'type61.inc'
INCLUDE 'type61.inc'
!local variables:
!local variables:
INTEGER Ipos,Jpos,Kpos,NnodeOpt (NoptMax)

```
    INTEGER Ipos,Jpos,Kpos,NnodeOpt (NoptMax)
```




```
    !Initialise NnodeOpt:
```

    !Initialise NnodeOpt:
    IF (Isim.LT.3) THEN
    IF (Isim.LT.3) THEN
    IF (IDE.EQ.1) THEN
    IF (IDE.EQ.1) THEN
    IF ((I.EQ.1).AND.(J.EQ.1).AND.(K.EQ.1)) THEN
    IF ((I.EQ.1).AND.(J.EQ.1).AND.(K.EQ.1)) THEN
    DO Iopt=1,Nopt
    DO Iopt=1,Nopt
        IF (INT(TypOpt(IOpt)/100).EQ. 1) THEN
        IF (INT(TypOpt(IOpt)/100).EQ. 1) THEN
            NnodeOpt(Iopt)=0
            NnodeOpt(Iopt)=0
            DO Ipos=PosOpt (Iopt, 1), PosOpt (Iopt, 4)
            DO Ipos=PosOpt (Iopt, 1), PosOpt (Iopt, 4)
            DO Jpos=PosOpt (Iopt, 2), PosOpt (Iopt, 5)
            DO Jpos=PosOpt (Iopt, 2), PosOpt (Iopt, 5)
            DO Kpos=PosOpt (Iopt, 3), PosOpt (Iopt, 6)
            DO Kpos=PosOpt (Iopt, 3), PosOpt (Iopt, 6)
            IF (TypSoil(Ipos,Jpos,Kpos).NE.0) THEN
            IF (TypSoil(Ipos,Jpos,Kpos).NE.0) THEN
                NnodeOpt (IOpt)=NnodeOpt(Iopt) +1
                NnodeOpt (IOpt)=NnodeOpt(Iopt) +1
            END IF
            END IF
            END DO
            END DO
            END DO
            END DO
            END DO
            END DO
        END IF
        END IF
        END DO
        END DO
        END IF
        END IF
        END IF
        END IF
        END IF
        END IF
    !Update Opt:
    !Update Opt:
    DO Iopt=1,Nopt
    DO Iopt=1,Nopt
    IF (INT (TypOpt (IOpt)/100).EQ.1) THEN
    IF (INT (TypOpt (IOpt)/100).EQ.1) THEN
        IF ((I.GE.PosOpt (Iopt,1)).AND.(I.&E.PosOpt(Iopt,4))) THEN
        IF ((I.GE.PosOpt (Iopt,1)).AND.(I.&E.PosOpt(Iopt,4))) THEN
        IF ((J.GE.PosOpt(Iopt,2)).AND.(J.LE.POSOpt(IOpt,5))) THEN
        IF ((J.GE.PosOpt(Iopt,2)).AND.(J.LE.POSOpt(IOpt,5))) THEN
        IF ((K.GE.PosOpt(IOpt,3)).AND.(K.LE.PosOpt(IOpt,6))) THEN
        IF ((K.GE.PosOpt(IOpt,3)).AND.(K.LE.PosOpt(IOpt,6))) THEN
            GOTO (101,102,103,104,105,106,107,108,109).
            GOTO (101,102,103,104,105,106,107,108,109).
    & (TypOpt(IOpt)-100)
    & (TypOpt(IOpt)-100)
            !Tsoil (degc)
            !Tsoil (degc)
            Opt(IOpt)=Opt(Iopt)+Tsoil2(I,J,K)/NnodeOpt(Iopt)/NDt
            Opt(IOpt)=Opt(Iopt)+Tsoil2(I,J,K)/NnodeOpt(Iopt)/NDt
            GOTO 999
            GOTO 999
            !Psoil(0) [kJ/hr]
            !Psoil(0) [kJ/hr]
            Opt (Iopt) =Opt (Iopt)+Psoil(0)*3.6*Nmod/NDt
            Opt (Iopt) =Opt (Iopt)+Psoil(0)*3.6*Nmod/NDt
            GOTO 999
            GOTO 999
            !Psoil(1) [kJ/hr]
            !Psoil(1) [kJ/hr]
            Opt (Iopt)=Opt(Iopt)+Psoil(1)*3.6*Nmod/NDt
            Opt (Iopt)=Opt(Iopt)+Psoil(1)*3.6*Nmod/NDt
            GOTO }99
    ```
            GOTO }99
```

```
2113
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2141
2142
2143
2145
146
2147
CONTINUE
END IF
END IF
END IF
END IF
END DO
RETURN
END
C******************************************************************************
C*****************************************************************************
    SUBROUTINE OptionalsMiscellaneous
    !common variables:
    !--------.------------
    INCLUDE 'type61.inc'
```



```
    IUpdate Opt:
    DO Topt=1 Nopt
    DO Iopt=1,Nopt
    IF (INT (TypOpt (IOpt)/100).EQ.2) THEN
        GOTO (201,202,203,204), (TypOpt(Iopt)-200)
        !PsuxfTot [kJ/hr]
        IF (IDT.EQ.NDT) Opt(Iopt)=PsurfTot*3.6
        GOTO }99
!PwatTot [kJ/hr]
        IF (IDT.EQ.NDT) Opt(Iopt)=PwatTot*3.6
        GOTO }99
        !PfricTot [kJ/hr]
        IF (IDT.EQ.NDT) Opt(Iopt)=PfricTot*3.6
        GOTO }99
        !PintTot [kJ/hr]
        IF (IDT.EQ.NDT) opt (Iopt)=pintTot*3.6
        CONTINUE
    END IF
    END DO
    RETURN
    END
C******************************************************************************
    FUNCTION Hsat$(T)
    !saturating pressure [Pa]
    !(Ashrare Handbook 1989, Ch.6, for -100<T<200 {degC])
        !local variables:
        !-------------------
        REAL HsatS,T,Tabs
    DATA Cn1,Cn2,Cn3,Cn4,Cn5,Cn6,Cn7 /
    & -5.6745359 E+3,
    & 6.3925247,
    & -9.677843 E-3,
    & 6.22115701 E-9,
    & 6 6.22115701 E-9,
```

```
    & -9.484024 E-13,
    4.163501/
    DATA Cp1,Cp2,Cp3,Cp4,Cp5,Cp7 /
    & -5.8002206 E+3,
    & 1.3914993.
        -4.8640239 E-2.
        4.1764768 E-5,
        -1.4452093 E-8,
        6.5459673/
```



```
        Tabs=MIN(MAX (T, -100.), 200.)+273.15
        IF (T.LT.0) THEN
        Hsat$=EXP(Cn1/Tabs+Cn2+Cn3*Tabs+Cn4*Tabs**2+Cn5*Tabs**3
    & +Cn6*Tabs**4+Cn7*LOG(Tabs))
        ELSE
        Hsat$=EXP(Cp1/Tabs+Cp2+Cp3*Tabs+Cp4*Tabs**2+Cp5*Tabs**3
    & +CP7*LOG(Tabs))
        END IF
        END
C******************************************************************************
C******************************************************************************
    FUNCTION Hrat$(PrWat, PrAir)
    !humidity ratio [ kg vapor/kg air]
    !(perfect gas equation)
    !common variables:
    !------------------
    REAL CmAix,CmWat,MmolAix,MmolWat, Rhowat,ClatWat,CmVap,Rgas
    COMMON/Type61PhysConst/
    &CmAir, CmWat, MmolAix,MmolWat, RhoWat, ClatWat, CmVap,Rgas
    !local vaxiables:
    !-----------------
    REAL Hrat$, PrWat, PrAir
```



```
    Hrat$=PrWat*MmolWat/(PrAir*MmolAir)
    END
C******************************************************************************
C*******************************************************************************
    FUNCTION Habs$(Hrat, PrAir)
    !absolute humidity of moist air [Pa]
    !(perfect gas equation)
    !common variables:
    REAL CmAir, CmWat,MmolAix, MmolWat, RhoWat, ClatWat, CmVap, Rgas
    COMMON/TYpe61PhysConst/
    &CmAir, CmWat, MmolAir, MmolWat, Rhowat, ClatWat, CmVap, Rgas
    !local variables:
    !----------------------
    REAL Habs$,Hrat, PrAir
```



```
    Habs$=Hrat*PrAir*MmolAir/MmolWat
    END
C*******************************************************************************
C******************************************************************************
    SUBROUTINE FindZero(Y,X,AZ,BZ,E2,K)
    !original name: NB02A (from NAG library)
    !determination of X +/- E2 so that Y(X)=0:
    !iterative calls to this routine allowsw to determinate }X\mathrm{ so that
    !
            AZ<X-E2< X < X+E2< BZ
    !where
    ! sgn(Y{AZ))=sgn(Y{X-E2})<> sgn(Y(X+E2))=\operatorname{sgn}(Y(BZ))
    !local variables:
    1------------------
    REAL Y ! value of Y(X) (computed outside of the routine): input
    REAL X ! value of X: output
    REAL AZ ! inferior value of interval: input
    REAL BZ ! superior value of interval: input
    REAL E2 ! precision: input
    INTEGER K ! state of determination:
        ! 0: initialisation
        : input
        1: iteration not completed
            : output
        2: iteration completed
        : output
        ! 3: inappropriate interval: sgn(Y(AZ))=sgn(Y(BZ))
```

```
        TF (K) 125,10,50
```

        TF (K) 125,10,50
    O
O
CALCULATE Y(X) AT X=AZ.
CALCULATE Y(X) AT X=AZ.
10 A = AZ
10 A = AZ
B=BZ
B=BZ
X = A
X = A
J1=1
J1=1
IT = 1
IT = 1
K=1
K=1
GO TO 20
GO TO 20
C
C
C BRANCH DEPENDING ON THE VALUE OF J1.
C BRANCH DEPENDING ON THE VALUE OF J1.
50 GO TO (60,120,170,170,170),J1
50 GO TO (60,120,170,170,170),J1
C
C
60 YA = Y
60 YA = Y
X=B
X=B
J1=2
J1=2
IT=2
IT=2
GO TO 20
GO TO 20
C
C
70 K=3
70 K=3
GO TO 20
GO TO 20
C
C
90 IT = IT+1
90 IT = IT+1
x= x2
x= x2
GO TO 20
GO TO 20
C
C
120 B = X
120 B = X
YB = Y
YB = Y
C MAKE TEST AT 200 FAIL IF YA OR YB ZERO
C MAKE TEST AT 200 FAIL IF YA OR YB ZERO
125 Y=AMAX1(ABS (YA), ABS (YB))*2.0
125 Y=AMAX1(ABS (YA), ABS (YB))*2.0
JI=3
JI=3
IF (YA*YB) 126,200,70
IF (YA*YB) 126,200,70
126 IF(K.GT.0)GO TO 100
126 IF(K.GT.0)GO TO 100
K=1
K=1
IT=0
IT=0
C
C
100 IF(B-A.LE.E2)GO TO 200
100 IF(B-A.LE.E2)GO TO 200
GO TO {10,10,130,150,160),.11
GO TO {10,10,130,150,160),.11
C
C
130 CALCULATE THE NEXT X BY THE SECANT METHOD BASED ON THE BRACKET
130 CALCULATE THE NEXT X BY THE SECANT METHOD BASED ON THE BRACKET
IF(ABS (YA) . LE.ABS (YB))GO TO 140
IF(ABS (YA) . LE.ABS (YB))GO TO 140
X1 = A
X1 = A
Y1 = YA
Y1 = YA
X = B
X = B
Y = YB
Y = YB
GO TO 150
GO TO 150
140 X1 = B
140 X1 = B
Y1 = YB
Y1 = YB
X = A
X = A
Y = YA
Y = YA
C
C
C USE THE SECANT METHOD BASED ON THE FUNCTION VALUES Y1 AND Y.
C USE THE SECANT METHOD BASED ON THE FUNCTION VALUES Y1 AND Y.
150 U=Y* (X-X1)/(Y-Y1)
150 U=Y* (X-X1)/(Y-Y1)
155 X2=X-U
155 X2=X-U
IF(X2.EQ.X)GO TO 110
IF(X2.EQ.X)GO TO 110
X1 = X
X1 = X
Y1 = Y
Y1 = Y
YTEST =.50*AMIN1(ABS (YA),ABS (YB))
YTEST =.50*AMIN1(ABS (YA),ABS (YB))
C
C
CHECK THAT X2 IS INSIDE THE INTEERVAL (A,B).
CHECK THAT X2 IS INSIDE THE INTEERVAL (A,B).
IF((X2-A)*(X2-B) .LT. 0.0)GO TO 90
IF((X2-A)*(X2-B) .LT. 0.0)GO TO 90
C
C
160 X2 = 0.50* (A+B)
160 X2 = 0.50* (A+B)
YTEST = 0.0
YTEST = 0.0
C
C
CHECK WHETHER THE MAXIMUM ACCURACY HAS BEEN ACHIEVED.
CHECK WHETHER THE MAXIMUM ACCURACY HAS BEEN ACHIEVED.
IF((X2-A)* (X2-B)) 90,200,200
IF((X2-A)* (X2-B)) 90,200,200
C
C
MOVE AWAY FROM EIXED POINT TO GET CLOSE BRACKET
MOVE AWAY FROM EIXED POINT TO GET CLOSE BRACKET
110 IF(U.EQ.0.0)GO TO 160
110 IF(U.EQ.0.0)GO TO 160
U=U+U
U=U+U
GO TO 155
GO TO 155
C
C
REVISE THE BRACKET (A,B)
REVISE THE BRACKET (A,B)
170 IF(Y.EQ.0.0)GO TO 195
170 IF(Y.EQ.0.0)GO TO 195
IF(YA*Y.GT.0.0)GO TO 180
IF(YA*Y.GT.0.0)GO TO 180
B = X
B = X
YB=Y

```
            YB=Y
```

```
        GO TO 190
    180 A = X
        YA = Y
C
C USE YTEST TO DECIDE THE METHOD FOR THE NEXT VALUE OF X.
    190 J1=4
        IF(ABS (Y) GT. YTEST I J1=5
        IF(YTEST .LE.0.0)J1=3
        GO TO 100
C
C Y = 0 - SET CLOSEST BRACKET
    195 IF (ABS (X-A).LT.ABS (X-B))GO TO 196
        A=X
        YA=Y
        GO TO 220
    196 B=X
        YB=Y
        GO TO 220
    200 IF(ABS(Y).LE.ABS(YB))GO TO 210
        X=B
        Y=YB
    210 IF (ABS (Y).LE.ABS (YA))GO TO 220
        X=A
        Y=YA
    220 K=2
    20 RETURN
        END
C******************************************************************************
C******************************************************************************
        SUBROUTINE SkipComment(FileUnit)
        llocal variables:
        !-------------------
        INTEGER FileUnit,ICar
        CHARACTER*256 String
        LOGICAL IsData
```



```
100 FORMAT(A256)
    IsData=.FALSE.
    DO WHILE (.NOT.IsData)
        READ(FileUnit,100) String
        IF (String(1:1).NE.**) THEN
            Icar=1
            DO WHILE ((.NOT.IsData).AND. {Icar.LE.256)}
                    IF (String(Icar:Icar).NE.' ') THEN
                    IsData=.TRUE.
                END IF
                ICar=Icar+1
            END DO
        END IF
        END DO
        BACKSPACE(FileUnit)
        RETURN
        END
C******************************************************************************
C******************************************************************************
    SUBROUTINE StopError(Ierr)
    !common variables:
    !-------------......--
    INCLUDE 'type61.inc
    !local variables:
    !--------m----------
    INTEGER IerrList(65), Igoto
    DATA (IerrList(Igoto), Igoto=1,65)
    & / 101, 102, 103, 104, 105, 106, 107, 201, 202, 203, 301, 401,
        402, 403, 404, 411, 412, 421, 422, 431, 434, 443, 444, 451,
        452, 501, 502, 503, 504, 505, 506, 601, 701, 702, 801, 802,,
        901, 902,903, 1001,1002,1101,1102,1201,1202,1203,1204,1205,
        1206,1301,1302,1303,1304,1305,1306,1401,1501,1502,1503,1504,
        1505,1506,2101,2201,9999/
```



```
1 FORMAT (A,6I4)
    WRITE(IparCon,1)'*!!!!!!!!!!!!!!!! (not completed) !!!!!!!!!!!!!!!!!!'
    WRITE(IparCon,1)
    WRITE(IparCon,1)'* TYPE 61 ERROR:',Ierr
    WRITE(Iparcon,1)
    Igoto=1
```


452 WRITE(Iparcon,1) :* TypSoil (I,J,NK)=0 at I, J: ©, I, J
WRITE(Iparcon,1) '* no tubes allowed on lower surface'
GOTO 9999
! Posinf
501 WRITE(IparCon,1) '* Posinf(1)<1 OR PosInf(1)>NI
GOTO 9999
502 WRITE(IparCon,1) '* PosInf(2)<1 OR PosInf(2)>NJ
GOTO 9999
503 WRITE(Iparcon, 1) '* Posinf (3)<1 OR PosInf(3)>NK'
GOTO 9999
504 WRITE(IparCon,1) '* PosInf(4)<POSInf(1) OR PosInf(4)>NI'
GOTO 9999
505 WRITE(Tparcon, 1) '* PosInf(5)<PosInf(2) OR PosInf(5)>NJ'
GOTO 9999
506 WRITE(IparCon,1) '* PosInf(6)<PosInf(3) OR PosInf (6) >NK.
GOTO 9999
! Kairo, Kairl

601 WRITE(IparCon, 1) , * Kair0<0 OR Kairl<0.
GOTO 9999
!LamSoil, CvSoil

701
GOTO 9999
WRITE(IparCon,1) '* CvSoil(Isoil)<=0 for Isoil:', Isoil
GOTO 9999
! LamTub, CvTub

801 WRITE(IparCon, 1) '* LamTub $<=0$ '
GOTO 9999
WRITE(IpaxCon,1) '* CvTub<=0'
GOTO 9999
IThTub, ctubcor
WRITE(Iparcon,1) '* ThTub<=0'
GOTO 9999
WRITE(IparCon,1) '* Ctubcor<=0'
GOTO 9999
903 WRITE(IparCon,1) '* Rfric<0'
GOTO 9999

1001 WRITE(IparCon,1) '* TypWat(Idir)<1 OR TypWat(Idir)>2'
WRITE(IparCon,1) '* for Idir:',Idir
GOTO 9999
1002 WRITE(IparCon,1) '* Vwat(Idir)<0 for Idir:',Idir
GOTO 9999
! NiniSoin, Niniwat

1101 WRITE(IparCon, 1) '* NiniSoil<1 OR NiniSoil>NiniMax'
GOTO 9999
1102 WRITE(IparCon,1) '* NiniWat<1 OR NiniWat>Ninimax'
GOTO 9999
!TiniSoil, PosIniSoil

1201
WRITE(Iparcon,1) '* PosIniSoil(Iini, 1)<1.
WRITE(Iparcon,1) '* OR'
WRITE(Iparcon,1) :* PosIniSoil(Iini,1)>NI'
GOTO 1299
WRITE(IparCon,1) '* PosIniSoil(Iini, 2)<1'
WRITE(Iparcon,1) '* OR'
WRITE(IparCon,1) '* PosIniSoil(Iini, 2) >NJ'
GOTO 1299
WRITE(Iparcon,1) '* PosIniSoil(Iini,3)<1'
WRITE(Iparcon,1) '* OR
WRITE(IparCon,1) '* PosIniSoil(Iini, 3)>NK'
GOTO 1299
1204 WRITE(IparCon,1) ** PosIniSoil(Iini, 4)<PosIniSoil(Iini, 1)'
WRITE(IparCon,1) '* OR'
WRITE(IparCon,1) '* PosIniSoil(Iini, 4) >NI'
GOTO 1299
1205 WRITE(IparCon,1) '* PosIniSoil(Iini,5)<PosIniSoil(Iini,2)'
WRITE(Iparcon,1) '* OR
WRITE(IparCon,1) '* PosIniSoil(Iini,5) $>\mathrm{NJ} '$
GOTO 1299
1206 WRITE (IparCon, 1) '* PosIniSoil(Iini,6)<PosIniSoil(Iini, 3)'
WRITE(Iparcon,1) '* OR'
WRITE(IparCon, 1) '* PosIniSoil(Iini, 6) $>\mathrm{NK}$ '
GOTO 1299

CND**********************************************************************

```
```


[^0]:    ' as evaluated by temperature gradient from 75 to 50 cm above as well as from 350 to 600 cm beneath pipes, with soil conductivities of 2.4 , respectively $2.2 \mathrm{~W} / \mathrm{K} \mathrm{m}$.
    ${ }^{2}$ as evaluated by temperature evolution at 50 cm above pipes, at interaxial position, as well as at 50,150 and 350 cm beneath pipes, with soil capacity above pipes of $2.5 \mathrm{MJ} / \mathrm{K} \mathrm{m}^{3}$, beneath pipes of $2.3 \mathrm{MJ} / \mathrm{K} \mathrm{m}^{3}$.

